

MEXICO OIL CONSERVATION COMM. ON
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12-7-73		DEC 13 1973	
Company Texaco Inc.				Connection Flared				O. C. C.	
Pool White City Penn				Formation Morrow				Unit ARTESIA, OFFICE	
Completion Date 12-3-73		Total Depth 11488		Plug Back TD 11435		Elevation 3365		Farm or Lease Name White City Comm	
Csg. Size 4.5	Wt. 13.50	d 3.920	Set At 11488	Perforations: From 11024 To 11354		Well No. 1			
Tbg. Size 2	Wt. 4.70	d 1.995	Set At 10900	Perforations: From To		Unit F	Sec. 33	Twp. 24	Rge. 26
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Gas						Packer Set At 10900		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 174 @ 11189		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State New Mexico	
L 11189	H 11189	G _g 0.577	% CO ₂ 1.18	% N ₂ 0.53	% H ₂ S 0.00	Prover	Meter Run 4.026	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3669	60			31
1.	4 x 2.00			120.6	6.3	54	3532	67			1.0
2.	4 x 2.00			250.2	10.2	35	3285	66			1.0
3.	4 x 2.00			303.0	13.0	29	3148	66			1.0
4.	4 x 2.00			360.6	16.0	29	2987	66			1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor F _{pv}	Rate of Flow Q, Mcfd
1	19.81	28.9	133.8	1.0058	1.316	1.011	767
2	19.81	51.9	263.4	1.0249	1.316	1.025	1423
3	19.81	64.0	316.2	1.0312	1.316	1.032	1776
4	19.81	77.3	373.8	1.0312	1.316	1.038	2159
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.	0.20	514	1.46	0.979	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	0.39	495	1.41	0.951	Specific Gravity Separator Gas 0.577 X X X X X X X X
3.	0.47	489	1.39	0.939	Specific Gravity Flowing Fluid _____ X X X X X 0.577
4.	0.55	489	1.39	0.928	Critical Pressure _____ P.S.I.A. 679 P.S.I.A.
5.					Critical Temperature _____ R 351 R

P _c 3682 P _c ² 13558.6				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{2.949}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{2.068}$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{4464}$		
1	12568.4	3549	12593.0	965.6			
2	10878.1	3309	10946.7	3611.9			
3	9993.2	3177	10095.3	3463.3			
4	9001.2	3024	9146.7	4411.9			
5							

Absolute Open Flow 4464 Mcfd @ 15.025		Angle of Slope θ 56.1	Slope, n .6718
Remarks: _____			
Approved By Commission:		Conducted By: R. E. Lee	Calculated By: Computer
		Checked By:	