

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Copy 631
C-122
Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 7/8/74		SEP - 5 1974	
Company TROPORO OIL & GAS COMPANY			Connection		
Well Cabin Lake <i>Morrow</i>			Location MORROW		
Date 7/8/74			Total Depth 13,950'		Perforations 13,802'
Casing Depth 7/8/74			Elevation 3331.2 GR		Form or Lease Name CABANA
Casing Size 4 1/2"	WT. 14.60#	Set At 13,950'	Perforations 13,660'-670' & 13,543' To 13,556'		Well No. //1
Casing Size 2 7/8" EUE	WT.	Set At 12,351'	Perforations 13,660'-670' & 13,543' To 13,556'		Unit Sec. Twp. Rge. N 1 - 22S - 30E
Type Well - Single - Broadhead - G.G. or G.O. Multiple			Packer Set At 12,351'		County EDDY
Producing Thru TUBING		Reservoir Temp. °F 184	Mean Annual Temp. °F 13607	Baro. Press. - P _a 60	State NEW MEXICO
L 13607	H 13607	G _g .586	% CO ₂	% N ₂	% H ₂ S
			PRCHOKE NIPPLE		

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI				3030		74	3030	74			
1.	2.0		13/64"	2990		76	2990	76			1 hr
2.	2.0		16/64"	2955		80	2955	80			1 hr
3.	2.0		20/64"	2820		76	2820	76			1 hr
4.	2.0		24/64"	2750		78	2750	78			1 hr
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcd
1.	.7238		3003.2	.9850	1.3063	1.123	3140.89
2.	1.087		2968.2	.9813	1.3063	1.119	4628.16
3.	1.672		2833.2	.9850	1.3063	1.129	6881.42
4.	2.378		2763.2	.9831	1.3063	1.119	9443.13
5.							

NO.	T _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcl/bbl.
1.	4.47	536	1.51	.793	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	4.42	540	1.53	.799	Specific Gravity Separator Gas _____ X X X X X X X X
3.	4.22	536	1.51	.705	Specific Gravity Flowing Fluid _____ X X X X X
4.	4.11	538	1.52	.798	Critical Pressure 672 P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature 354 R _____ R

NO.	P _w	P _w ²	P _w ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{9261}{451}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 5.3996$
1.	3003.2	9019.	242	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 24.990$	
2.	2968.2	8810.	451		
3.	2833.2	8027.	1234		
4.	2763.2	7635.	1626		
5.					

Absolute Pressure 24,990	Mcd @ 15.025	Angle of Slope @ 60 50Min.	Slope, n .558
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Remarks: **ONE STEPWISE CALCULATION HAS BEEN MADE BUT DUE TO LARGE VOLUMES, SURFACE PRESSURES DO NOT SHOW ENOUGH DROP SO OBSERVED SURFACE PRESSURES HAVE BEEN PLOTTED.**

Approved by Commission:	Conducted By: J. Spruill	Calculated By: J. Spruill	Checked By: Nolan Brunson, Jr.
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