Weatherford Copy to SF 2102

NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
JUL 12 1974
O. C. C.
ARTESIA, OFFICE

Type Test: ☒ Initial ☐ Annual ☐ Special			Test Date: 6-28-74	
Company: MOBIL OIL CORP	Connection: —			
Pool: SOUTH CARLSBAD MORROW	Formation: MORROW			Unit: 320
Completion Date: 6-18-74	Total Depth: 12235'	Plug Back TD: 12234	Elevation:	Farm or Lease Name: BINDEL COM.
Csg. Size: 7" / Wt.: 26# / d: 6.276 / Set At: 12234		Perforations: From 12100' To 12114		Well No.: 1
Tbg. Size: 2 3/8 / Wt.: N-80 / d: 1.995 / Set At: 12095		Perforations: From To		Unit: J / Sec.: 4 / Twp.: 23-S / Rge.: 27-E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE		Packer Set At: 12075		County: EDDY
Producing Thru: TUBING	Reservoir Temp. °F: 191 @ 12107	Mean Annual Temp. °F: 60°	Baro. Press. – P_a: 13.2	State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
12309	12107	0.602	1.8	0.7	0		4"	FLANGE

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					3549		265	–	27 HRS
1.	4 X 1.5	350	5	72	1390	60	265	–	1 HR
2.	4 X 1.5	610	7	84	1100	60	265	–	1 HR
3.	4 X 1.5	600	12	92	715	60	265	–	1 HR
4.	4 X 1.5	590	15	97	620	60	265	–	1 HR
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	10.84	42.61	363.2	0.9794	1.2888	1.0257	5721
2.	10.84	66.04	623.2	0.9776	1.2888	1.0438	941.7
3.	10.84	85.72	613.2	0.9705	1.2888	1.0405	1210.3
4.	10.84	95.12	603.2	0.9662	1.2888	1.0323	1333.2
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	0.53	542	1.53	0.950
2.	0.91	544	1.54	0.917
3.	0.90	552	1.56	0.923
4	0.88	557	1.58	0.927
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas 0.602 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX 0.602
Critical Pressure 678 P.S.I.A. 678 P.S.I.A.
Critical Temperature 352 R 352 R

P_c _____ P_c^2 12687.2

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	19689	1407.2	1980.3	10706.9
2	12392	1126.3	1268.6	11420.6
3	5302	762.5	581.4	12107.8
4	4002	681.0	463.8	12225.4
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.184$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.717$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1625.7$

Absolute Open Flow 1625.7 Mcfd @ 15.025 Angle of Slope θ 9.631 Slope, n 5.292

Remarks: SUBJECT WELL IS TOO WEAK TO GET BETTER TEST ∴ 421

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
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