

ULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Revised 9-1-65

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B-122

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 7-19-74		AUG 5 1974							
Company Coquina Oil Corp.		Connection		O. C. C. ARTESIA, OFFICE							
Pool So. Carlsbad		Formation Morrow		Unit							
Completion Date 7-19-74		Total Depth 11,940		Plug Back TD 11,940							
Csg. Size 7"		Wt. 35#		Elevation 3356KB							
Tub. Size 2 7/8		Wt. 6.5		Farm or Lease Name Philly Federal							
Set At 11,940		Perforations: From 11,824 To 11,836		Well No. 1							
Set At 11,771		Perforations: From To		Unit Soc. Twp. Rge. H 21 23S 26E							
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 11,771							
Producing Thru tubing		Reservoir Temp. °F 203.0 11,800		Mean Annual Temp. °F 60							
		Baro. Press. - P _a 13.2		State New Mexico							
L 11,771		H 11,771		Gg .625							
		% CO ₂ None		% N ₂ None							
		% H ₂ S None		Prover 4.026							
				Meter Run Flange							
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. in. H ₂ O	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							3999				
1.	4.026		2.50	610	4.6	64	3971	74			60 min.
2.	4.026		2.50	630	11	78	3938	75			60 min.
3.	4.026		2.50	520	37	58	3847	75			60 min.
4.	4.026		2.50	710	39	48	3829	75			60 min.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1	32.64	53.54	623.2	.9962	1.265	1.063	2,340				
2	32.64	84.11	643.2	.9831	1.265	1.057	3,664				
3	32.64	140.46	533.2	1.002	1.265	1.054	6,125				
4	32.64	167.94	723.2	1.012	1.265	1.075	7,544				
5											
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry gas	Mcft/bbl.				
1	.92	524	1.43	.895	A.P.I. Gravity of Liquid Hydrocarbons	None	Deq.				
2	.95	538	1.47	.895	Specific Gravity Separator Gas	.625	X X X X X X X X				
3	.79	518	1.42	.900	Specific Gravity Flowing Fluid	X X X X X					
4	1.07	508	1.39	.866	Critical Pressure	671	P.S.I.A.				
5					Critical Temperature	365	R				
NO.	P _t	P _w	P _w ²	P _t ² - P _w ²	(1) $\frac{P_t^2}{P_t^2 - P_w^2} = 23.64$	(2) $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 5.5394$					
1		5036.2	25363	172	ACF = Q $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 41,789$						
2		5024.2	25243	292							
3		4979.2	24792	743							
4		4945.2	24455	1080							
5											
Approved by Commission:	Conducted By:	Calculated By:	Checked By:								
	J. Spruell	J. Spruell	B. Pyle								