

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT ONE POINT BACK PRESSURE TEST GAS WELL

Copy 6.51
Form C-122
Revised 9-1-65 -122

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 8-5-75		SEP 19 1975	
Company Grace Oil Company					Connection		O. C. C.	
Pool Undesignated <i>Sheep Draw</i> <i>2-5204 4-20-74</i>					Formation Strawn		UNIT ARTESIA, OFFICE Cueva Unit	
Completion Date 9/4/75		Total Depth 11,577		Plug Back TD 11512		Elevation 3418.7		Farm or Lease Name Cueva Unit
Csg. Size 5 1/2	Wt. 17#	Set At 11,618	Performance From 10,255 To 10,264	Well No. 1				
Tbg. Size 2 3/8	Wt.	Set At 10,092	Perforations: From To	Unit K	Sec. 6	Twp. 23S	Rge. 26E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple					Packer Set At 10,092		County Eddy	
Producing Thru Tbg.		Reservoir Temp. °F 135° @ 10092	Mean Annual Temp. °F 60°	Baro. Press. - P _a 13.2		State New Mexico		
L 10092	H 10092	Gg .585	% CO ₂	% N ₂	% H ₂ S	Prover 2"	Meter Run	Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3821			76	
1.	2"	x	3/32	3770		58	3770	58		76	60 min.
2.	2"	x	1/8	3476		52	3476	52		78	60 min.
3.	2"	x	3/16	2840		68	2840	68		84	60 min.
4.	2"	x	1/4	2100		82	2100	82		84	60 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	.1867		3770	1.002	1.307	1.090	1005
2.	.3506		3476	1.008	1.307	1.121	1800
3.	.8052		2840	.9924	1.307	1.131	3355
4.	1.4390		2100	.9795	1.307	1.137	4399
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry gas	Mcf/bbl.
1.	5.61	518	1.48	.841	A.P.I. Gravity of Liquid Hydrocarbons	Dry	
2.	5.17	512	1.46	.796	Specific Gravity Separator Gas	.585	XXXXXXXXXX
3.	4.23	528	1.51	.782	Specific Gravity Flowing Fluid	XXXXX	Dry gas
4.	3.13	542	1.55	.774	Critical Pressure	672	P.S.I.A.
5.					Critical Temperature	350	R

NO.	P _c ²	P _w ²	R _w ²	P _c ² - R _w ²	(1) $\frac{P_c^2}{P_c^2 - R_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n =$
1	3783.2	14313	388		1.44	.342
2	3489.2	12175	2526			
3	2853.2	8141	6560			
4	2113.2	4466	10235			
5						

Absolute Open Flow		15080	Mcf/d @ 15.025	Angle of Slope	62°	Slope, n	.531
Remarks:							
Approved By Commission:		Conducted By: <i>John Brooks</i>		Calculated By: <i>David Carruth</i>		Checked By:	