NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
JUL 30 1975
O. C. C.
ARTESIA, OFFICE

Type Test: [x] Initial [ ] Annual [ ] Special				Test Date: 7-24-75	
Company: Samedan Oil Corporation			Connection: None		Unit: 320
Pool: Undesignated			Formation: Morrow Gas		
Completion Date: 7-24-75	Total Depth: 11805		Plug Back TD: 11744	Elevation: 3306'KB	Farm or Lease Name: Carlsbad State Com.
Csg. Size: 4½	Wt: 13.5 / 11.6	d: 3.920 / 4.000	Set At: 11794	Perforations: From 11410 To 11732	Well No.: 1
Tbg. Size: 2 3/8	Wt.: 4.7	d: 1.995	Set At: 11315	Perforations: From Open ended To	Unit: B; Sec.: 34; Twp.: 23s; Rge.: 26e
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Duel G.G.			Packer Set At: 11315		County: Eddy
Producing Thru: Tbg	Reservoir Temp. °F: 204 @ 11271	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11571	–	0.581	1.353	0.284	0.00	x	–	

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g. DWT	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						3072		Packer		72.0
1.	2	18/64 1.250	113	–	53	2331	77			1.0
2.	2	16/64 1.250	102	–	52	2435	79			1.0
3.	2	15/64 1.250	93	–	52	2592	79			1.0
4.	2	14/64 1.250	85	–	55	2737	80			1.0
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	27.63	–	126.2	1.007	1.312	–	4606.8
2.	27.63	–	115.2	1.008	1.312	–	4209.5
3.	27.63	–	106.2	1.008	1.312	–	3880.6
4.	27.63	–	98.2	1.005	1.312	–	3577.6
5.							

NO.	P_t	Temp. °R	T_r	Z
1	0.19	513	1.49	–
2.	0.17	512	1.49	–
3.	0.16	512	1.49	–
4.	0.14	515	1.50	–
5.				

Gas Liquid Hydrocarbon Ratio: Dry Gas Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: – Deg.
Specific Gravity Separator Gas: 0.581 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 679 P.S.I.A. – P.S.I.A.
Critical Temperature: 344 R – R

P_c 3926.2 P_c^2 15415.0

NO	P_t^2	P_w*	P_w^2	$P_c^2 - P_w^2$
1		3422.2	11711.5	3703.5
2		3483.2	12132.7	3282.3
3		3538.2	12518.9	2896.1
4		3578.2	12803.5	2611.5
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.162$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.81$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 12945$

Absolute Open Flow: 12945 Mcfd @ 15.025 Angle of Slope θ: 54°14' Slope, n: 0.721

Remarks: * BHP @ (-8265) 11571' used for pressure calculations

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Coleman Petr. Engr. Co.	Joe A. Coleman	Joe A. Coleman