

NE MEXICO OIL CONSERVATION COMMS. V
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7-14-75		JUL 30 1975	
Company Samedan Oil Corporation				Connection None		O. C. C.	
Pool Undesignated				Formation Strawn Gas		Unit ARTESIA, OFFICE	
Completion Date 7-14-75		Total Depth 11805		Plug Back TD 11744		Elevation 3306'KB	
Csg. Size 4 1/2		Wt. 13.5		Set At 11794		Perforations: From 10354 To 10370	
Thq. Size 2 3/8		Wt. 4.7		Set At 10275		Perforations: Open Ended From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10175		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 180 @ 10200		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
L 10362		H -		G _g 0.604		% CO ₂ 0.682	
				% N ₂ 0.710		% H ₂ S 0.000	
				Prover X		Meter Run -	
						Taps -	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Time Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	DWT	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2517			Packer		72.0
1.	2 17/64	1.250	3	-	28	1715	76					1.0
2.	2 14/64	1.000	10	-	41	1790	78					1.0
3.	2 10/64	1.000	7	-	56	1825	78					1.0
4.	2 6/64	1.000	6	-	92	1920	79					1.0
5.												

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	27.63	-	16.2	1.032	1.287	-	594.5
2	17.09	-	23.2	1.019	1.287	-	520.0
3	17.09	-	20.2	1.004	1.287	-	446.1
4	17.09	-	18.2	0.9706	1.287	-	388.5
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 243.650 Mcf/bbl.	
1	0.02	488	1.38	-	A.P.L. Gravity of Liquid Hydrocarbons 52.3	
2	0.03	501	1.42	-	Specific Gravity Separator Gas 0.604	
3	0.03	516	1.46	-	Specific Gravity Flowing Fluid XXXXX	
4	0.03	552	1.56	-	Critical Pressure 674 P.S.I.A.	
5					Critical Temperature 354 R	

NO.	P _t ²	P _w * ²	P _w ²	P _c ² - P _w ²	$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.719$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.698$ $AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1009$
1	2094.2	4385.7	6100.2		
2	2233.2	4987.2	5498.7		
3	2411.2	5813.9	4672.0		
4	2547.2	6488.2	3997.2		

Absolute Open Flow 1009 Mcfd @ 15.025		Angle of Slope @ 45° 39'	Slope, n 0.978
Remarks: * BHP @ (-7056) 10362' used for pressure calculations			
Approved By Commission:	Conducted By: Coleman Petr. Engr. Co.	Calculated By: Joe A. Coleman	Checked By: Joe A. Coleman