

WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURES ( $P_w$  or  $P_s$ )

Form C-122F  
Adopted 9-1-65

FROM KNOWN BOTTOM HOLE PRESSURE ( $P_b$  or  $P_s$ )

COMPANY Belco Den. LEASE Jarvis Road WELL NO. 1 DATE 1-26-84

LOCATION: Unit N Section 5 Township 22 S Range 27 E

L 11044 H 11044 L/H 1.00 G .592 % CO<sub>2</sub> 1.259 % N<sub>2</sub> .319 % H<sub>2</sub>S \_\_\_\_\_

GH 6538  $P_{CT}$  676  $T_{CT}$  353  
TABLE IX & X

DATE I DATE II DATE III DATE IV

| LINE | 1                                                      | 2       | 3       | 4       | 5       | 6       | 7       | 8      |
|------|--------------------------------------------------------|---------|---------|---------|---------|---------|---------|--------|
| 1    | $T_w(W.H. \cdot R)$                                    | 534     | 534     | 534     | 534     | 534     | 534     | 534    |
| 2    | $T_s(B.H. \cdot R)$                                    | 644     | 644     | 644     | 644     | 644     | 644     | 644    |
| 3    | $T = (\frac{T_w + T_s}{2})$                            | 589     | 589     | 589     | 589     | 589     | 589     | 589    |
| 4    | Z (Est.)                                               | .927    | .900    | .906    | .884    | .886    | .868    | .850   |
| 5    | TZ                                                     | 546     | 530     | 534     | 521     | 521     | 512     | 505    |
| 6    | GH/TZ                                                  | 11.97   | 12.33   | 12.51   | 12.56   | 12.53   | 12.77   | 12.94  |
| 7    | $e^S$ (Table XIV)                                      | 1.57    | 1.59    | 1.58    | 1.60    | 1.60    | 1.61    | 1.62   |
| 8    | $P_b$ or $P_s$                                         | 4191.2  | 4191.2  | 3870.2  | 3870.2  | 3531.2  | 3531.2  | 3160.2 |
| 9    | $P_f^2$ or $P_s^2$                                     | 17566.2 | 17566.2 | 14978.4 | 14978.4 | 12469.4 | 12469.4 | 9986.9 |
| 10   | $P_c^2 = P_f^2 / e^S$ or $P_w^2 = P_s^2 / e^S$         | 11211.5 | 11061.5 | 9460.9  | 9353.3  | 7794.8  | 7723.5  | 6182.4 |
| 11   | $P_b$ or $P_w$                                         | 3348.3  | 3325.9  | 3075.8  | 3058.3  | 2791.9  | 2779.1  | 2486.4 |
| 12   | $P = (\frac{P_w + P_s}{2})$ or $(\frac{P_c + P_f}{2})$ | 3769.8  | 3758.5  | 3473.0  | 3464.3  | 3161.6  | 3155.2  | 2823.3 |
| 13   | $P_r = (P/P_G)$                                        | 5.58    | 5.56    | 5.14    | 5.13    | 4.68    | 4.67    | 4.17   |
| 14   | $T_r = (T/T_G)$                                        | 1.67    | 1.67    | 1.67    | 1.67    | 1.67    | 1.67    | 1.67   |
| 15   | Z (Table XI)                                           | .900    | .899    | .884    | .883    | .869    | .868    | .858   |