

c/SF
File

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED BY

O. C. D.
ARTESIA, OFFICE

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 1-23-84	
Company Belco Development Corp. ✓		Connection Llano	
Pool South Carlsbad <i>MOR</i>		Formation <i>Atoka MOR</i>	
Completion Date 1-17-84		Total Depth 12,478	Plug Back TD 11,070
		Elevation 3141 Gl.	Farm or Lease Name Jarvis Mead <i>Cont.</i>
Csg. Size 7"	Wt. 23#	d 6.366	Set At 11,784
		Perforations: From 11,036 To 11,053	
Thq. Size 2 7/8"	Wt. 6.5#	d 2.411	Set At 10,791
		Perforations: From OPENENDED To	
Type Well - Single - Brdenhead - G.C. or G.O. Multiple Single		Packer Set At 10,791	Well No. 1
Producing Thru Tubing		Reservoir Temp. °F 184° 11,044	Mean Annual Temp. °F 60°
		Baro. Press. - P _a 13.2	Unit Sec. Twp. Rge. N 5 22S 27E
L 11,044		H 11,044	Cg .5923
		% CO ₂ 1.259	% N ₂ .319
		% H ₂ S	Prover Meter Run 3"
			Tape Flange
FLOW DATA			
NO.	Prover Line Size	X	Orifice Size
SI			
1.	3	x	1.500
2.	3	x	1.500
3.	3	x	1.500
4.	3	x	1.500
5.			
TUBING DATA			
	Press. p.s.i.g.	Temp. °F	Duration of Flow
	3517	61°	72 Hr
	3300	61	1 Hr
	3050	62	1 Hr
	2737	62	1 Hr
	2390	63	1 Hr
CASING DATA			
	Press. p.s.i.g.	Temp. °F	Duration of Flow
	PKR	CHOKE	72 Hr
		7/64	1 Hr
		9.5/64	1 Hr
		11.5/64	1 Hr
		14/64	1 Hr
RATE OF FLOW CALCULATIONS			
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m
1	11.13	68.01	578.2
2	11.13	117.29	573.2
3	11.13	152.74	583.2
4	11.13	191.78	593.2
5			
NO.	R _f	Temp. °R	T _f
1	.86	539	1.53
2	.85	536	1.52
3	.86	534	1.51
4	.88	532	1.51
5			
Z			
1	.921		
2	.920		
3	.917		
4	.915		
5			
Gas Liquid Hydrocarbon Ratio _____ Mcl/bbl.			
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.			
Specific Gravity Separator Gas .592			
Specific Gravity Flowing Fluid XXXXX			
Critical Pressure 676 P.S.I.A.			
Critical Temperature 353 R			
P _c 3540.7 P _c ² 12533.0			
NO.	P _i ²	P _w	P _w ²
1		3325.9	11061.6
2		3058.3	9353.2
3		2779.1	7723.4
4		2479.5	6147.9
5			
(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.963$			
(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.611$			
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.618$			
Absolute Open Flow 4,618 Mcl @ 15.025			
Angle of Slope 54.75			
Slope, n .707			
Remarks: Calculated from known bottom hole pressures, measured with Kuster Gauge.			
Approved By Commission:		Conducted By: W.S.	Calculated By: R.R.
			Checked By: R.R.