

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST F

GAS WELL

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 8-30-78		SEP 11 1978	
Company Amoco Production Company ✓				Connection El Paso Natural Gas Company			
Pool Undesignated Strawn <i>Und. Strawn</i>				Formation Strawn <i>Strawn</i>		Unit ARTESIA, OFFICE	
Completion Date		Total Depth 13255.		Plug Back TD 13226.		Elevation 3031	
Csg. Size 5.000		WT. 18.0		Set At 4.267		Perforations: From 11484. To 11491.	
Tub. Size 2.875		WT. 6.5		Set At 2.441		Perforations: From 0 To 0	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single				Packer Set At 11015		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 189 @ 11488		Mean Annual Temp. °F 60.0		Boro. Press. - P _g 13.2	
L 11488		H 11488		G _g 0.616		% CO ₂ 0.40	
				% N ₂ 0.75		% H ₂ S 0	
				Prover 0		Meter Run 6.1	
						Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3312	65			43.5
1.	6.06 x 4.000			610	4.0	53	2840	69	0	0	1.0
2.	6.06 x 4.000			612	9.0	82	2488	69	0	0	1.0
3.	6.06 x 4.000			630	16.8	110	1910	70	0	0	1.0
4.	6.06 x 4.000			632	23.0	88	1694	70	0	0	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _L	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mscf
1	85.37	49.93	623.2	1.0068	1.2741	1.0603	5797
2	85.37	75.01	625.2	0.9795	1.2741	1.0488	8382
3	85.37	103.95	643.2	0.9551	1.2741	1.0410	11241
4	85.37	121.82	645.2	0.9741	1.2741	1.0484	13532
5							

NO.	P _i	Temp. °R	T _i	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.93	513	1.42	0.889	93.4	56.0	0.616		672	361
2	0.93	542	1.50	0.909						
3	0.96	570	1.58	0.923						
4	0.96	548	1.52	0.910						
5										

NO.	P _i	P _w	P _i ²	P _w ²	P _i ² - P _w ²
1	8141	2913	8486	2537	
2	6256	2650	7022	4001	
3	3699	2250	5062	5960	
4	2763	2184	4771	6252	
5					

(1) $\frac{P_i^2}{P_i^2 - P_w^2} = 1.7630$

AOF = Q $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 23104$

(2) $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 1.7074$

Absolute Open Flow	23104	Mscf @ 15.025	Angle of Slope @	46.7	Slope, n	0.943
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Remarks:

Approved By Commission:	Conducted By: John West Engineering	Calculated By: CCW	Checked By: RMB
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