

NEV EXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 6-19-80		JUN 30 1980		
Company AMOCO PRODUCTION COMPANY ✓					Connection EL PASO NATURAL GAS COMP		O. C. D.		
Pool WILDCAT N. LOVING					Formation ATOKA		Unit ARTESIA, OFFICE		
Completion Date 1/03/80		Total Depth 12664.		Plug Back TD 11965.		Elevation 3062.		Farm or Lease Name CARTER GAS COM	
Csg. Size 4.500	Wt. 13.5	d 3.920	Set At 12664.	Perforations: From 11176. To 11186.			Well No. 1		
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 11080.	Perforations: From 11193. To 11203.			Unit Sec. Twp. Rge. J 18 23S 28E		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE					Packer Set At 10147.		County EDDY		
Producing Thru TUBING		Reservoir Temp. °F 175 @ 11190.		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2		State NEW MEXICO	
L 11190.	H 11190.	Gg 0.620	% CO ₂ 0.42	% N ₂ 1.29	% H ₂ S 0.	Provor 0.	Meter Run 4.0	Taps FLANGE	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Provor Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3600.	92.			44.5
1.	4.00 X 1.000			175.	4.0	100.	3530.	94.	0.	0.	0.5
2.	4.00 X 1.000			440.	14.4	100.	3350.	91.	0.	0.	1.0
3.	4.00 X 1.000			580.	27.0	100.	2885.	94.	0.	0.	1.0
4.	4.00 X 1.000			580.	59.3	100.	2350.	95.	0.	0.	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.75	27.44	188.2	0.9636	1.2698	1.0129	162.
2	4.75	80.90	453.2	0.9636	1.2698	1.0312	485.
3	4.75	126.65	593.2	0.9636	1.2698	1.0408	767.
4	4.75	187.54	593.2	0.9636	1.2698	1.0408	1135.
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.28	560.	1.55	0.975	44.8 Mcf/bbl.	64.0 Deg.	0.620	XXXXXX	671. P.S.I.A.	361. R
2	0.68	560.	1.55	0.940				XXXXXX	668. P.S.I.A.	378. R
3	0.88	560.	1.55	0.923						
4	0.88	560.	1.55	0.923						
5										

P _c 3565.9 P _c ² 12716.				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	12554.	3494.	12207.	509.
2	11311.	3317.	11005.	1711.
3	8400.	2851.	8130.	4586.
4	5585.	2318.	5373.	7343.
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.7317$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4931$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1695.$

Absolute Open Flow 1695. Mcfd @ 15.025

Angle of Slope θ 53.9

Slope, n 0.730

Remarks:			
Approved By Commission:	Conducted By: JOHN WEST ENGINEERING	Calculated By: REGENA WHITTEN	Checked By: LARRY SHEPPARD

3 - NMOC D-A 1-Hou 1-Susp 1-DLB 1-LWS