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NEW EXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR JUNE 1980

Form C-122
Revised 9-1-65

O. C. D.

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5-30-80					ARTESIA, OFFICE				
Company AMOCO PRODUCTION COMPANY					Connection EL PASO NATURAL GAS COM									
Pool WILDCAT					Formation MORROW					Unit F				
Completion Date 12/13/79			Total Depth 10826.			Plug Back TD 10780.			Elevation 3910.			Farm or Lease Name STATE HK COM		
Csg. Size 5.500	Wt. 15.5	d 4.950	Set At 10826.	Perforations: From 10640. To 10655.			Well No. 1							
Thg. Size 2.375	Wt. 4.7	d 1.995	Set At 10262.	Perforations: From 0. To 0.			Unit L 6 24S 25E							
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE					Packer Set At 10197.					County EDDY				
Producing Thru TUBING			Reservoir Temp. °F 161. @ 10648.			Mean Annual Temp. °F 60.0			Baro. Press. - P _a 13.2			State NEW MEXICO		
L 10648.	H 10648.	Gg 0.575	% CO ₂ 0.91	% N ₂ 0.19	% H ₂ S 0.	Prover 0.	Meter Run 4.0	Taps FLANGE						

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3313.	66.			42.2
1.	4.00 X 1.500			452.	11.6	124.	2332.	68.	0.	0.	1.0
2.	4.00 X 1.500			458.	19.0	112.	2127.	69.	0.	0.	1.0
3.	4.00 X 1.500			463.	21.2	100.	1995.	69.	0.	0.	0.7
4.	4.00 X 1.500			469.	43.6	82.	1509.	68.	0.	0.	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	10.85	73.33	465.2	0.9436	1.3188	1.0230	1012.
2	10.85	94.59	471.2	0.9535	1.3188	1.0255	1323.
3	10.85	100.38	476.2	0.9636	1.3188	1.0281	1422.
4	10.85	144.93	482.2	0.9795	1.3188	1.0327	2097.
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.69	584.	1.68	0.956	0.	0.	0.575	XXXXXX	677.	349.
2.	0.70	572.	1.64	0.951						
3.	0.70	560.	1.61	0.946						
4.	0.71	542.	1.55	0.938						
5.										

P _c 3321.5 P _c ² 11032.				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	5500.	2345.	5498.	5534.
2	4580.	2143.	4594.	6438.
3	4033.	2015.	4059.	6973.
4	2317.	1554.	2414.	8618.
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2801$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2684.$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.2801$

Absolute Open Flow	2684.	Mcfd @ 15.025	Angle of Slope θ	45.0	Slope, n	1.000
Remarks:						
Approved By Commission:		Conducted By: John West Eng.		Calculated By: Regena Whitten		Checked By: L. W. Sheppard

0-3 NMOC-D-A 1-Hou 1-Susp 1-WDM 1-DLB