

NEW EXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST, OR GAS WELL

Form C-122
Revised 9-1-65
RECEIVED

MAY 11 1981

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 4- 4-81		MAY 11 1981	
Company AMOCO PRODUCTION COMPANY				Connection EL PASO NATURAL GAS COMP		O. C. D. ARTESIA, OFFICE	
Pool South Rock Tank UNDESIGNATED				Formation SOUTH ROCK TANK MORROW		Unit	
Completion Date 10-18-80		Total Depth 10850.		Plug Back TD 10230.		Elevation 3874.	
Csg. Size 5.500		Wt. 15.5		Set At 4.950		10849.	
Tbg. Size 2.375		Wt. 4.7		Set At 1.995		9814.	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 9752.		County EDDY	
Producing Thru TUBING		Reservoir Temp. °F 174.0 10217.		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2	
L 10217.		H 10217.		G _g 0.578		% CO ₂ 0.69	
				% N ₂ 0.68		% H ₂ S 0.	
				Prover 0.		Meter Run 4.0	
						Taps FLANGE	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3070.	53.			46.0
1.	4.00 X 1.250			590.	1.0	63.	3032.	54.	0.	0.	0.5
2.	4.00 X 1.250			590.	4.8	63.	2985.	56.	0.	0.	0.5
3.	4.00 X 1.250			590.	6.7	59.	2952.	57.	0.	0.	0.5
4.	4.00 X 1.250			605.	14.4	49.	2881.	58.	0.	0.	0.5
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	7.47	24.56	603.2	0.9971	1.3149	1.0471	252.
2.	7.47	53.81	603.2	0.9971	1.3149	1.0471	552.
3.	7.47	63.57	603.2	1.0010	1.3149	1.0487	656.
4.	7.47	94.35	618.2	1.0107	1.3149	1.0540	987.
5.							

NO.	R ₁	Temp. °R	T ₁	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.89	523.	1.50	0.912	0.578	XXXXXXX
2.	0.89	523.	1.50	0.912	0.578	XXXXXXX
3.	0.89	519.	1.49	0.909	675.	675. P.S.I.A.
4.	0.92	509.	1.46	0.900	349.	349. P.S.I.A.
5.						

P _c 3093.3 P _c ² 9569.				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 8.3634$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6.4433$	
NO.	P ₁ ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6362.$		
1	9273.	3054.	9329.	240.			
2	8989.	3006.	9036.	533.			
3	8792.	2972.	8835.	734.			
4	8376.	2903.	8425.	1144.			
5							

Absolute Open Flow		6362.	Mcf/d @ 15.025	Angle of Slope θ	48.7	Slope, μ	0.877
Remarks:							
Approved By Commission:		Conducted By:		Calculated By:		Checked By:	
		John West Engineering		R. Whitten		L. W. Sheppard	