

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 11-20-80		DEC 3 1980	
Company AMOCO PRODUCTION COMPANY				Connection EL PASO NATURAL GAS COMP			O. C. D.	
Pool UNDESIGNATED				Formation MORROW			Unit ARTESIA, OFFICE	
Completion Date 7 29 80		Total Depth 10950.		Plug Back TD 10907.		Elevation 4037.		Form or Lease Name STATE IC COM
Csg. Size 5.500	Wt. 15.5	d 4.950	Set At 10949.	Perforations: From 10830. To 10842.			Well No. 1	
Thq. Size 2.375	Wt. 4.7	d 1.995	Set At 10751.	Perforations: From 0. To 0.			Unit Sec. Twp. Rge. C 7 24S 25E	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple SINGLE				Packer Set At 10711.			County EDDY	
Producing Thru TUBING		Reservoir Temp. °F 178.8 10836.		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2		State NEW MEXICO
L 10836.	H 10836.	G _g 0.576	% CO ₂ 0.94	% N ₂ 0.47	% H ₂ S 0.	Prover 0.	Meter Run 4.0	Taps FLANGE

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							4136.	58.			51.7
1.	4.00 X 1.250			490.	29.2	73.	2592.	59.	0.	0.	1.0
2.	4.00 X 1.250			475.	41.0	70.	2332.	60.	0.	0.	1.0
3.	4.00 X 1.250			460.	53.3	72.	2255.	59.	0.	0.	1.0
4.	4.00 X 1.250			458.	72.2	93.	1924.	59.	0.	0.	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	7.47	121.13	503.2	0.9877	1.3177	1.0363	1221.
2	7.47	141.41	488.2	0.9905	1.3177	1.0359	1428.
3	7.47	158.80	473.2	0.9887	1.3177	1.0344	1599.
4	7.47	184.51	471.2	0.9697	1.3177	1.0291	1813.
5.							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.74	533.	1.53	0.931	0.	0.	0.576	XXXXXX	677.	348.
2.	0.72	530.	1.52	0.932				XXXXXX		
3.	0.70	532.	1.53	0.935						
4.	0.70	553.	1.59	0.944						
5.										

P _c 4154.4 P _c ² 17259.					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.2872$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.2872$	
NO	P _i ²	P _w	P _c ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2333.$	
1	6787.	2617.	6847.	10412.		
2	5500.	2359.	5565.	11694.		
3	5145.	2286.	5227.	12032.		
4	3753.	1962.	3851.	13408.		
5						

Absolute Open Flow	2333.	Mcfd @ 15.025	Angle of Slope θ	45.0	Slope, n	1.000
Remarks:						
Approved By Commission:		Conducted By: John West Eng.		Calculated By: Chris Van Dooren		Checked By: Larry Sheppard

3-NMOC-D-A · 1-Hou 1-Susp 1-DLB 1-LWS