NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122
Revised 4-1-65

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
DEC 9 1980
O. C. D.
ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 11/28/80

Company: AMINOIL USA, INC.	Connection: AIR		Unit: F
Pool: ~~UNDESIGNATED~~ malaga atoka	Formation: ATOKA		
Completion Date: 11/22/80	Total Depth: ~~12,744~~ 12746	Plug Back TD: 11,743	Elevation: 3018 G.L.
Csg. Size / Wt. / d / Set At:		Perforations: From 11,617 To 11,632	Farm or Lease Name: VASQUEZ Com.
Tbg. Size: 2 7/8 / Wt. / d / Set At: 11,515		Perforations: From To	Well No.: 1
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE GAS		Packer Set At: 11,515	Unit: F; Sec.: 3; Twp.: 24s; Rge.: 28e
Producing Thru: TBG.	Reservoir Temp. °F: 189 @ 11,515	Mean Annual Temp. °F: 60	County: EDDY
		Baro. Press. – P_a: 13.2	State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11,515	11,515	.580	.012	.017			4"	FLG.

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI					2060				72 HR
1.	4 X 2.500	475	2.0	91	1950				45 MIN
2.	4 X 2.500	480	4.0	80	1925				45 MIN
3.	4 X 2.500	490	8.0	68	1750				1 Hr
4.	4 X 2.500	490	14.0	71	1700				1 HR
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	32.64	31.25	488.2	.9715	1.313	1.033	1344
2	32.64	44.42	493.2	.9813	1.313	1.035	1933
3	32.64	63.45	503.2	.9924	1.313	1.039	2804
4	32.64	83.93	503.2	.9896	1.313	1.038	3695
5							

NO.	P_t	Temp. °R	T_r	Z
1	.73	551	1.57	.938
2	.73	540	1.54	.933
3	.75	528	1.51	.927
4	.75	531	1.52	.928
5				

Gas Liquid Hydrocarbon Ratio: DRY Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: .580 XXXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 672 P.S.I.A. P.S.I.A.
Critical Temperature: 350 R R

P_c 2073.2 P_c^2 4298.2

NO	BHP	P_w	P_w^2	$P_c^2 - P_w^2$
1	2567.2	2005.8	4023.4	274.8
2	2510.2	1961.9	3848.9	449.3
3	2439.2	1906.9	3636.3	661.9
4	2358.2	1844.7	3402.8	895.4
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.800$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 4.281$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 15.818$

Absolute Open Flow: 15,818 Mcf/d @ 15.025 Angle of Slope θ: 47.25° Slope, n: .927

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	DAVIS SERVICES, INC.	RICK PAGAN	