

MEXICO OIL CONSERVATION COM. ON
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

ckf
File

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 11-14-88		NOV 29 '88	
Company GREAT WESTERN DRILLING CO.				Connection NONE					
Pool DARK CANYON PENN-GAS UNDESIGNATED				Formation STRAWN				Unit O. C. D. ARTESIA, OFFICE	
Completion Date 11-09-88		Total Depth 10,102		Plug Back TD 10,065		Elevation 3824 Gr.		Farm or Lease Name MOSLEY SPRINGS "32"	
Csq. Size 4 1/2	Wt. 11.6#	d 3.820"	Set At 10,102	Perforations: From 9,566 To 9,588		Well No. 124 State Court			
Thq. Size 2 3/8	Wt. 4.7	d 1.995	Set At 9,522"	Perforations: From OPEN To ENDED		Unit Sec. Twp. Rye. N 32 23S 25E			
Type Well - Single - Bradenhead - G.C. or G.O. Multiple SINGLE						Packer Set At 9,487		County EDDY	
Producing Thru TUBING		Reservoir Temp. °F 190 @ 9,563		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State N.M.	
L 9,563	H 9,563	Gg .642	% CO ₂ .35	% N ₂ .66	% H ₂ S 0	Prover	Meter Run 4.026	Taps FLG.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3162		PKR		24
1.	4 X 1.500			450	6.00	77	2752		"		1 HR.
2.	4 X 1.500			460	11.00	75	2495		"		1 HR.
3.	4 X 1.500			465	18.00	70	2208		"		1 HR.
4.	4 X 1.500			470	36.00	64	1594		"		1 HR.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	10.84	52.72	463.2	.9840	1.248	1.041	731
2.	10.84	72.14	473.2	.9859	1.248	1.048	1,008
3.	10.84	92.78	478.2	.9905	1.248	1.048	1,302
4.	10.84	131.89	483.2	.9962	1.248	1.049	1,865
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	102.5 Mcf/bbl.
1.	.69	537	1.44	.922	A.P.I. Gravity of Liquid Hydrocarbons	57.4 @ 60° Deg.
2.	.71	535	1.43	.910	Specific Gravity Separator Gas	.642 X X X X X X X X
3.	.71	530	1.42	.910	Specific Gravity Flowing Fluid	X X X X X
4.	.72	524	1.40	.909	Critical Pressure	670 P.S.I.A.
5.					Critical Temperature	372 R

P _c 3239.6 P _c ² 10495.0				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.418$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.418$	
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.645$		
1	*	2825.3	7982.3	2512.7			
2	*	2538.6	6444.5	4050.5			
3	*	2251.4	5068.8	5426.2			
4	*	1759.2	3094.8	2400.2			
5							

Absolute Open Flow		2.645	Mcf @ 15.025	Angle of Slope @	45	Slope, n	1.000
Remarks: WELL MADE 2.00 BBLS 57.4° @ 60 CONDENSATE & .80 BBLS H ₂ O. TEST CALCULATED BY KNOWN BHP'S.							
Approved By Commission:		Conducted By: W.S.		Calculated By: B.M.		Checked By: B.M.	

Post #0-2
12-9-88
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