

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

APR 12 '90

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 4-8-90			
Company MERIDIAN OIL INC. ✓				Connection VENTED		AREA OFFICE	
Pool Mosley BALDRIDGE CANYON STRAWN				Formation STRAWN		Unit	
Completion Date 4-4-90		Total Depth 10740		Plug Back TD 10102		Elevation KB 4136	
Form or Lease Name JURNEGAN ST. COM.				Well No. 1			
Csq. Size 4 1/2	Wt. 18	d 4,000	Set At 11740	Perforations: From 9369' To 9476'			
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 9256	Perforations: From OPEN To END		Unit Sec. Twp. Rge. XL 12 24-S 24-E	
Type Well - Single - Straddlehead - G.C. or G.C. Multiple SINGE				Packer Set At 9250'		County EDDY	
Producing Thru TGB		Reservoir Temp. °F 176° @ 10203'		Mean Annual Temp. °F 13.2		State N.M.	
L 10203	H 10203	Gg .592	% CO ₂ .57	% N ₂ .53	% H ₂ S	Prover	Meter Run 4.026
						Taps FLG	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. in. Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						2505		PK		24
1.	4 X 1.250			390	12.00	52	2400	"		1 HR
2.	4 X 1.250			660	44.00	115	2030	"		"
3.	4 X 1.250			665	68.00	120	1580	"		"
4.	4 X 1.250			820	85.00	120	1188	"		"
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_{LP}}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mscf/d
1	7.469	69.56	403.2	1.008	1.300	1.041	709
2	7.469	172.11	673.2	.9510	1.300	1.041	1,654
3	7.469	214.75	678.2	.9469	1.300	1.041	2,055
4	7.469	266.12	833.2	.9469	1.300	1.051	2,572
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	NO CONDENSATE	Mcf/bbl.
1.	.60	512	1.44	.923	A.P.I. Gravity of Liquid Hydrocarbons	N/A	Deg.
2.	1.00	575	1.62	.923	Specific Gravity Separator Gas	592	XXXXXXX
3.	1.01	580	1.63	.922	Specific Gravity Flowing Fluid	XXXXX	
4.	1.24	580	1.63	.906	Critical Pressure	672	P.S.I.A.
5.					Critical Temperature	354	R

NO.	P _r ²	P _w ²	P _r ²	P _r ² - P _w ²	(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 1.342$	(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.196$
1		2415.8	5836.0	505.3	AOF = Q $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 3.076$	
2		2059.8	4242.6	2098.7		
3		1625.5	2645.6	3695.7		
4		1271.7	1617.1	4724.2		
5						

Absolute Open Flow	3,076	Mscf @ 15.025	Angle of Slope θ	59	Slope, n	.609
--------------------	-------	---------------	------------------	----	----------	------

Remarks: WELL MADE 2.00 BBL H2O DURING TEST

Approved By Division	Conducted By JOHN WEST ENGINEERING	Calculated By B.M.	Checked By B.M.
----------------------	---------------------------------------	-----------------------	--------------------