

NEW MEXICO OIL CONSERVATION COMMISSION
 MULTIPHASE AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

RECEIVED

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 3-23-81		MAY 1 1981		
Company Yates Petroleum Corporation			Connection El Paso Natural Gas Company				
Pool Crooked Creek Morrow			Formation Morrow		Unit ARTESA GROUP		
Completion Date 10-17-80		Total Depth 10707 KB		Plug Back TD 10613 KB	Elevation 4194 KB	Farm or Lease Name Lechuguilla Canyon Unit	
Casing Size 4 1/2"	Wt. 11.6#	d 4.000"	Set At 10699KB	Perforations: From 10476 To 10484		Well No. 8	
Tubg. Size 2 3/8"	Wt. 4.7#	d 1.995"	Set At 10440KB	Perforations: From To		Unit Sec. Twp. Rge. K 10 24s 24e	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single				Packer Set At 10440		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 163 @ 10480		Mean Annual Temp. °F 62		Baro. Press. - P _a 13.2	
L 10470		H 10470	G _g 0.589	% CO ₂ 1.34	% N ₂ 0.19	% H ₂ S N.7	
					Prover --	Meter Run 4	
						Taps Flanged	
FLOW DATA							
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	
SI							
1.	4.026	X	1.250	595	5	77	
2.	4.026	X	1.250	596	9	77	
3.	4.026	X	1.250	608	21	76	
4.	4.026	X	1.250	611	31	76	
5.							
						Duration of Flow 21 hrs. 24 hrs. 24 hrs. 24 hrs.	
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	
1	7.469	55.15	608.2	.9840	1.305	1.044	
2	7.469	74.05	609.2	.9840	1.305	1.044	
3	7.469	114.22	621.2	.9850	1.305	1.045	
4	7.469	139.10	624.2	.9850	1.305	1.046	
5						1397	
NO.	R _f	Temp. °R	T _f	z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.		
1	.898	537	1.532	.9176	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.		
2	.899	537	1.532	.9175	Specific Gravity Separator Gas 0.587 XXXXXXXXXX		
3	.917	536	1.529	.9151	Specific Gravity Flowing Fluid XXXXX 0.589		
4	.921	536	1.529	.9147	Critical Pressure 677.5 P.S.I.A. 826 P.S.I.A.		
5					Critical Temperature 350.5 R 405.5 R		
P _c 4187.2	P _c ² 17533						
NO	P _i ²	P _w	R _w ²	P _c ² - R _w ²	(1) $\frac{P_c^2}{P_i^2 - P_w^2} = 2.0437$		
1		3968.4	15748	1785	(2) $\left[\frac{P_c^2}{P_i^2 - R_w^2} \right]^n = 1.5228$		
2		3814.6	14551	2982			
3		3359.5	11286	6247			
4		2992.4	8954	8579	AOF = Q $\left[\frac{h_t^2}{P_c^2 - R_w^2} \right]^n = 2127$		
5							
Absolute Open Flow 2127			Mcid @ 15.025		Angle of Slope @ 59.5 deg.		
					Slope, n 0.5884		
Remarks: Static BHP extrapolated from BHP build up by Bennett Wireline, tubing pressures from DWT. Well gradually cleaned up on sales line.							
Approved By Commission:		Conducted By: Tracy Richardson		Calculated By: Eddie Mahfood		Checked By:	