STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
P O BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL.

Type Test: ☒ Initial FOUR POINT ☐ Annual ☐ Special			Test Date: 4-28-81		NW¼ NE ¼ RECEIVED
Company: COQUINA OIL CORP		Connection: AIR NEW WELL			MAY 6 1981
Pool: ~~DUBIN~~ RANCH Atoka		Formation: ATOKA			Unit: E O. C. D.
Completion Date: 4-22-81	Total Depth: 12,700	Plug Back TD: 11,668	Elevation:		Farm or Lease Name: HARROUN COMM ARTESIA, OFFICE
Csg. Size: 7.	Wt.: 38.	d:	Set At: 11,668	Perforations: From 11,462 To 11,471	Well No.: 1
Tbg. Size: 2.375	Wt.: 6.5	d:	Set At: 11,295	Perforations: From OPEN To ENDED	Unit: E Sec.: 33 Twp.: 22S Rge.: 28E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE			Packer Set At: 11,295		County: EDDY
Producing Thru: TUBING	Reservoir Temp. °F: 198 @ 11,470	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2		State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11,466.5	11,466.5	.5770	.427	.789	0		4"	FLG

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: BHP p.s.i.g.	Temp. °F	Duration of Flow
SI					5732	80	7014.		141.5
1.	4 X 1½	505	12.0	94	5023.	72	6251		1
2.	4 X 1½	520	24.0	86	4607.	74	5793		1
3.	4 X 1½	530	39.0	80	4024.	76	5143		1
4.	4 X 1½	535	58.0	73	3377.	77	4421		1
5.	4 X 1½	515	42.0	80	3158.	76	4180		6

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.12	78.86	518.2	.9688	1.3165	1.0314	1154
2	11.12	113.12	533.2	.9759	1.3165	1.0342	1671
3	11.12	145.55	543.2	.9813	1.3165	1.0370	2168
4	11.12	178.31	548.2	.9877	1.3165	1.0386	2678
5	11.12	148.94	528.2	.9813	1.3165	1.0353	2215

NO.	P_t	Temp. °R	T_r	Z
1	.77	554	1.60	.940
2	.79	546	1.58	.935
3	.81	540	1.56	.930
4	.81	533	1.54	.927
5	.78	540	1.56	.933

Gas Liquid Hydrocarbon Ratio .5554 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 88.2 Deg.
Specific Gravity Separator Gas .5770 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 673 P.S.I.A. ____ P.S.I.A.
Critical Temperature 345 R ____ R

P_c 7027.2 P_c^2 49381.5

NO	P_w	P_w^2	$P_c^2 - P_w^2$
1	6264.2	39240.2	10141
2	5806.2	33712	15670
3	5156.2	26586.4	22795
4	4434.2	19662.1	29719
5	4193.2	17582.8	31799

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.6616$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.4823$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3969.7$

Absolute Open Flow 3969.7 Mcfd @ 15.025 | Angle of Slope θ 52.2 | Slope, n .7752

Remarks: STABLIZED OPEN FLOW POTENTIAL 3,115.7 MCFD, ANGLE OF SLOPE 52.2
SLOPE N .7752 KNOWN BOTTOM HOLE PRESSURES FROM TANDUM AMERADA BOMBS.

Approved By Division	Conducted By:	Calculated By:	Checked By:
	DON BENNETT	WOHLFORD & JENKINS	