

RECEIVED

Type Well: ☒ Initial ☐ Annual ☐ Special						NOV 13 1981	
Company: PERRY R. PASS				Fluid: Air		O. C. B.	
Location: Southwest Indian Flats, Wildcat				Middle Morrow		ARTESIA, OKLAHOMA	
Completion Date: Oct. 20, 1981				2129		Big Eddy Unit	
Orif. Size: 5 1/2	Wt.: 17#	Orif. No.: 12729	Orif. No.: 12191	Orif. No.: 82			
Trq. Size: 2 3/8	Wt.: L.7#	Orif. No.: 12140			Unit: 10		22s 28E
Type well - Single - Perforated - Gas or Oil Multiple: Single Gas				12140		County: Eddy	
Producing Int. Tbg.		Reservoir Temp. °F: 196	Mass Avg. H. Temp. °F: 60	13.2		State: New Mexico	
L: *12172	H: 12172	G _g : .5961	% CO ₂ : 2.152	.802		Enter Item: 4"	Flg.

FLOW DATA							TUBING		GASING DATA		Duration of Flow
NO.	Prover Line Size	Orif. Size	Press. (psig)	Diff. (in)	Temp. (°F)	Flow (gpm)	Length (ft)	Press. (psig)	Temp. (°F)		
51						4120				72 hrs.	
1.	4 X 1.250		450	6.5	97	3970				1 hrs.	
2.	4 X 1.250		455	16.0	102	3820				1 hrs.	
3.	4 X 1.250		475	47.0	91	3415				1 hrs.	
4.	4 X 1.250		720	64.0	100	2925				1 hrs.	
5.	4 X 1.750		470	33.0	93	2620				4 hrs.	

NO.	Coefficient (24 Hour)	$\sqrt{V_{WFm}}$	Pressure P _L	Flow Temp. (°F)	Gravity Factor	Super. Viscosity Factor, F _{sv}	Rate of Flow Q, Mcf.
1	7.469	34.87	453.2	966.2	.29	1.030	528
2	7.469	36.55	468.2	9615	.29	1.030	829
3	7.469	31.43	488.2	9715	.29	1.034	1472
4	7.469	26.62	733.2	9566	.29	1.047	2114
5	14.93	126.28	483.2	9653	.29	1.031	2430

NO.	P _t	Temp. °F	g	Z	Com. Lib. H ₂ O Cond. at Bottom	API Gravity at 60°F	Specific Gravity at 60°F	Specific Gravity at 60°F	Critical Temp. °F	Critical Pressure psia
1	.68	557	1.57	.943						
2	.69	562	1.58	.943						
3	.72	551	1.55	.936						
4	1.08	560	1.58	.913						
5	.71	558	1.57	.940						

Q = 4133.2 gpm

NO. BHP: 5014.2, 4830.2, 4356.2, 3792.2, 3614.2

5188.2 S.I.P.

(1) $\frac{P_t}{P_b} = \frac{1.08}{1.0} = 1.08$

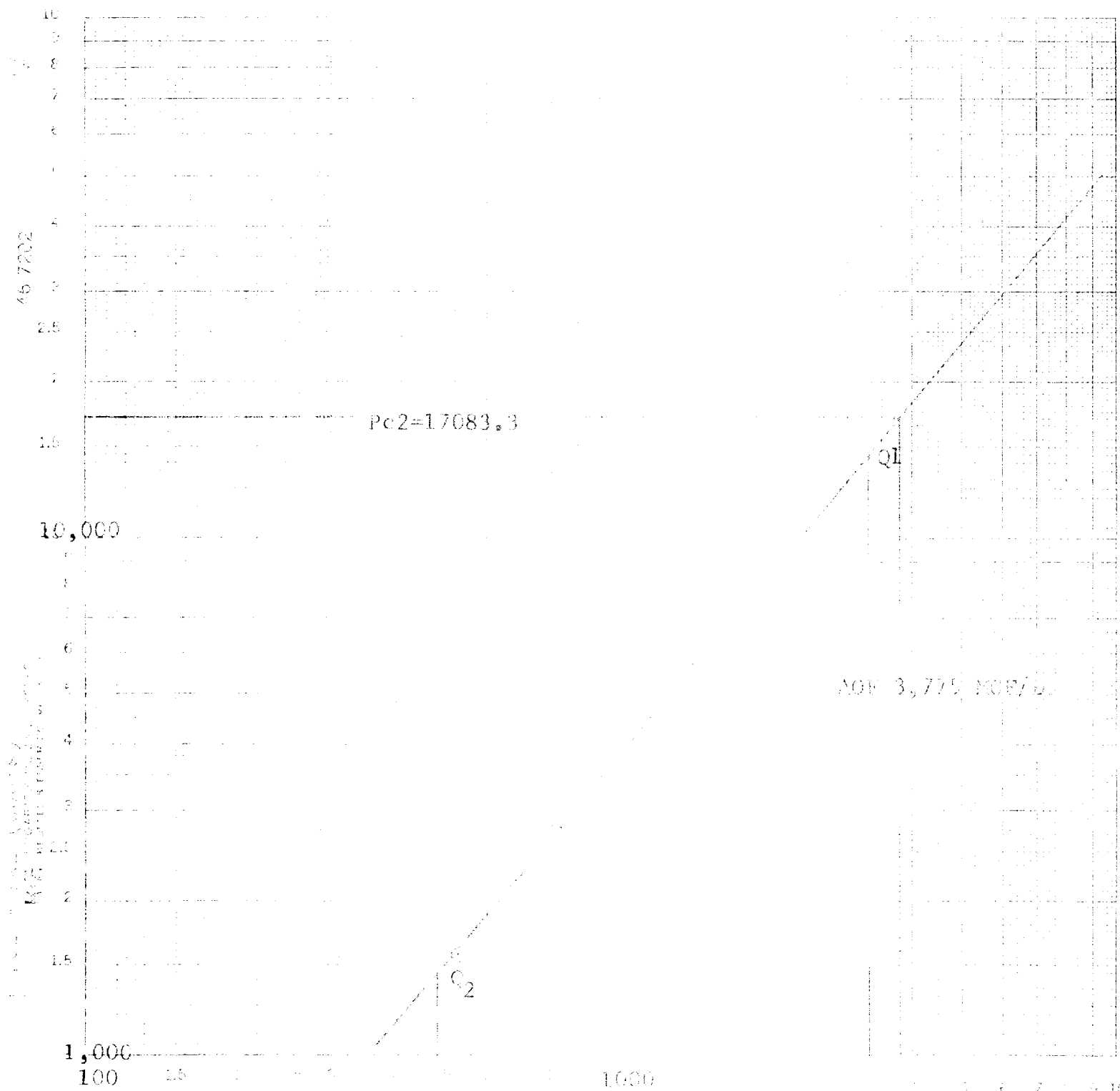
$\left[\frac{P_t}{P_b} \right]^n = 1.786$

Absolute Gas Flow: 3,775	Angle of Inclination: 30°	Correction: .837
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Remarks: * Pressure obtained from a bottom-hole pressure set at 12172 ft.
1 bbl. of H₂O was produced during the test.

Approved by: [Signature]	Conducted by: Davis Services, Inc. Rio	Checked by: [Signature]
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COMPANY : PLURY R. DAVIS
 LEASE : BIG EDDY 111
 WELL NO. : 11
 UNIT : SEC-10/TWP-22S/R-13E
 COUNTY : TULSA
 STATE : NEW MEXICO
 DATE : 10/20/87



AGE 3,775 MCF/D

$Q = MCF/D$
 $Q1 = 23.0; \log of 1 = 1.3513$
 $Q2 = 4.0; \log of 2 = 0.3010$

WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURES (~~P_w~~ or P_w)
FROM KNOWN BOTTOM HOLE PRESSURE (~~P_s~~ or P_s)

Form C-122F
Adopted 9-1-65

COMPANY Bass Enterprises LEASE Big Eddy Unit WELL NO. 82 DATE 10-20-81

LOCATION: Unit _____ Section 10 Township 22S Range 28E

L. 12172 H 12172 L/H 1.000 G .5961 %CO₂ 2.152 %N₂ .802 %H₂S _____

GH 7256 P_{cr} 679 T_{cr} 355
TABLE IX & X

LINE	1st Rate	2nd Rate	3rd Rate	4th Rate
1	T _w (W.H. °R)	534	534	534
2	T _s (B.H. °R)	656	656	656
3	T _c ($\frac{T_w + T_s}{2}$)	595	595	595
4	Z (Est.)	.984	.946	.970
5	TZ	585.5	562.9	577.2
6	GH/TZ	12.393	12.891	12.572
7	e ^s (Table XIV)	1.592	1.622	1.602
8	P _f or P _s	5014.2	5014.2	4830.2
9	P _f ² or P _s ²	25142.2	25142.2	23330.8
10	P _{c2} = P _f ² /e ^s or P _{w2} = P _s ² /e ^s	15796.8	15504.6	14560.7
11	P _c or P _w	3974.5	*3937.6	3815.8
12	P _c ($\frac{P_w + P_s}{2}$) or ($\frac{P_c + P_f}{2}$)	4494.4	4475.9	4323.0
13	P _r = (P/P _{cr})	6.62	6.59	6.37
14	T _r = (T/T _{cr})	1.68	1.68	1.68
15	Z (Table XI)	.946	.945	.934

WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURES ~~K_s~~ or P_w)

Form C-122F
Adopted 9-1-65

FROM KNOWN BOTTOM HOLE PRESSURE ~~K_s~~ or P_s)

COMPANY Bass Enterprises LEASE Big Eddy Unit WELL NO. 82 DATE 10-20-81

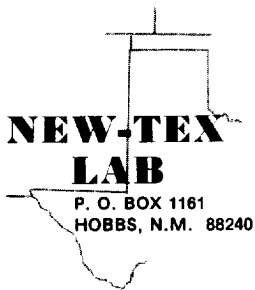
LOCATION: Unit 12172 Section 10 Township 22s Range 28E

L 12172 H 12172 L/H 1.000 G .5961 % CO₂ 2.152 % N₂ .802 % H₂S

GH 7256 P_{cr} 679 T_{cr} 355
TABLE IX & X TABLE IX & X

5th Rate

	1	2	3	4	5	6	7	8
1 T _w (W.H. °R)	534	534						
2 T _s (B.H. °R)	656	656						
3 T = ($\frac{T_w + T_s}{2}$)	595	595						
4 Z (Est.)	.890	.869						
5 TZ	529.6	517.1						
6 GH/TZ	13.702	14.033						
7 e ^s (Table XIV)	1.672	1.693						
8 P _f or P _s	3614.2	3614.2						
9 P _f ² or P _s ²	13062.4	13062.4						
10 P _c ² - P _f ² /e ^s or P _w ² = P _s ² /e ^s	7814.0	7717.6						
11 P _c or P _w	2795.4	*2778.1						
12 P _c - ($\frac{P_w + P_s}{2}$) or ($\frac{P_c + P_f}{2}$)	3204.8	3196.1						
13 P _f = (P/P _{cr})	4.72	4.71						
14 T _f = (T/T _{cr})	1.68	1.68						
15 Z (Table XI)	.869	.869						



CERTIFICATE OF ANALYSIS

No. _____
Run No. _____
Date of Run _____
Date Secured _____

A Sample of _____
Secured from _____
At _____ Secured by _____
Time _____ Date _____
Sampling conditions _____ Press _____
Temp. _____
Station No. _____

FRACTIONAL ANALYSIS

Percentage Composition

MOL % LIQ. % G.P.M.

Carbon Dioxide	_____	_____	_____
Air	_____	_____	_____
Nitrogen	_____	_____	_____
Oxygen	_____	_____	_____
Hydrogen sulfide	_____	_____	_____
Hydrogen	_____	_____	_____
Methane	_____	_____	_____
Ethane	_____	_____	_____
Propane	_____	_____	_____
Butanes	_____	_____	_____
Iso-Butane	_____	_____	_____
N-Butane	_____	_____	_____
Pentanes	_____	_____	_____
Iso-Pentane	_____	_____	_____
N-Pentane	_____	_____	_____
Hexanes	_____	_____	_____
Heptanes	_____	_____	_____
Octanes	_____	_____	_____
TOTAL	_____	_____	_____

Calc. Sp. Gr. _____
Calc. A.P.I. _____
Calc. Vapor Press. _____ PSIA
Sp. Gr. _____
Mol. Wt. _____

LIQUID CONTENT (GAL./MCF)

Propane Calc. G.P.M. _____
Butanes Calc. G.P.M. _____
Pentanes Plus. G.P.M. _____
Ethane Calc. G.P.M. _____
_____ # RVP Gasoline G.P.M. _____
B.T.U./Cu. Ft. @ 14.696 P.S.I.A.
Dry Basis _____
Wet Basis _____
Sulfur Analysis by Titration
Gr./100 Cu. Ft. _____
Hydrogen Sulfide _____
Mercaptans _____
Sulfides _____
Residual Sulfur _____
Total Sulfur _____

Run by _____ Checked by _____ Approved by _____

Additional Data and Remarks

