Gas Production

B.T. Gauge Numbers		7303			Ticket Numb e r		956649		
			PRESSURE	PRESSURE	4				
			8025.3	8070.0	·	ration	1st Flow	3220	
Final Hydrostatic		8009.4	8035.0	A Production 2nd Elo			-	M	
	Initial	Time	1691.8	1644.4		Rate	3rd Flow	4175	M
1st Flow (Final 30		1949.2		e Size		-	M
	Closed In Pressure			7434.0	<u></u>	age Tested		6.5	i
2nd Flow	Initial			1098.4		-		5	
		Final 90		1844.4		Weight Viscosity		13.4	ibs./gol
	Closed In Pressure			7344.0		Gravity		.031	
	Initial				1			<u>Est65</u>	· ·
3rd Flow	Final					Gas Compressibility Temperature		1.20	
	Closed In Pressure					iperature		182	
Extrapolated	· · · · · · · · · · · · · · · · · · ·	İst	7447	7400					
Static Pressure 2nd			7447	7460			· · · · ·		
		3rd							
Slope P/10		<u>lst</u>	-					_	
		2nd	6928	6941					
	1	3rd	-						
Remarks:					<u> </u>			<u> </u>	
		•							
	SUMMAR	Y	B.T. Gauge Depth	N₀. 7303 1116		B.T. Gaug Depth		02 230'	<u> </u>
PRODUCT			-	No. 7303 1116 SECOND					י טאו
PRODUCT Transmissibi	EQUA Kh 1637 0		Depth	1116	2'	Depth	112	230' THIRE	
	$\frac{EQUA}{\mu} = \frac{1637 Q}{m}$ $Kh = \frac{Kh}{\mu} = \frac{Kh}{\mu}$	TION	Depth	1116 SECOND	2'	Depth	112 	230' THIRE	md. f
Transmissibi Theoretical Flow Capaci Average	$\frac{EQUA}{\mu} = \frac{1637 Q}{m}$ $Kh = \frac{Kh}{\mu} = \frac{Kh}{\mu}$	TION	Depth	1116 second 705.742	2'	Depth	112 SECOND 704.468	230' THIRE	md. f
Transmissibi Theoretical Flow Capaci	$\frac{EQUA}{\mu} = \frac{1637 Q}{m}$ $\frac{Kh}{\mu} = \frac{1637 Q}{m}$ $\frac{Kh}{\mu} = \frac{Kh}{\mu} - \mu$ $\frac{Kh}{K_1} = \frac{Kh}{h}$	TION 0, ZT	Depth	1116 second 705.742	2'	Depth	112 SECOND 704.468 21.839	230' THIRE	md. f
Transmissibi Theoretical Flow Capaci Average Effective	$\frac{EQUA}{\mu} = \frac{1637 Q}{m}$ $\frac{Kh}{\mu} = \frac{1637 Q}{m}$ $\frac{Kh}{\mu} = \frac{Kh}{\mu} - \mu$ $\frac{Kh}{\mu} = \frac{Kh}{h}$ $\frac{K_1 = \frac{Kh}{h}}{K_1 = \frac{Kh}{h}}$ $\frac{Kh}{\mu} = \frac{3200 Q_e \mu}{\mu}$	ZT Log(0.472 b s ² - Pr ²	Depth FIRST	1116 SECOND 705.742 21.878	2'	Depth	112 SECOND 704.468 21.839 -	230' THIRE	<u>md. 1</u> cp md. 1 md.
Transmissibi Theoretical Flow Capaci Average Effective Permeability Indicated Flo Capacity	$EQUA$ $EQUA$ $\frac{EQUA}{\mu} = \frac{1637 \text{ Q}}{\text{m}}$ $\frac{Kh}{\mu} = \frac{1637 \text{ Q}}{\text{m}}$ $\frac{Kh}{\mu} = \frac{Kh}{\mu}$ $\frac{Kh}{\mu} = \frac{Kh}{h}$ $K_1 = \frac{Kh}{h}$ $K_1 = \frac{Kh}{h}$ $\frac{3200 \text{ Q}_{e} \mu}{\text{ P}}$ $\frac{Kh}{\text{ I}} = \frac{1600 \text{ F}}{1000 \text{ G}}$	TION zT_{o} ZT_{o} zT_{o}	Depth FIRST	1116 second 705.742 21.878 - 4.376	2'	Depth	112 SECOND 704.468 21.839 - 4.368	230' THIRE	<u>md. 1</u> cp md. 1 md.
Transmissibi Theoretical Flow Capaci Average Effective Permeability Indicated Flo Capacity Damage Rat	$\frac{EQUA}{\mu} = \frac{EQUA}{m}$ $\frac{Kh}{\mu} = \frac{1637 Q}{m}$ $\frac{Kh}{\mu} = \frac{Kh}{\mu} \mu$ $\frac{K}{\mu} = \frac{Kh}{h}$ $\frac{K_{1} = \frac{Kh}{h}}{K_{1} = \frac{Kh}{h}}$ $\frac{Kh}{\mu} = \frac{3200 Q_{e} \mu}{P}$ $\frac{Kh}{h} = \frac{1600 P}{P}$ $\frac{Kh}{h} = \frac{1000 P}{P}$	TION $p_r ZT$ ZT Log(0.472 b) $r_s^2 - P_r^2$ $r_s^2 - P_r^2$ $r_s^2 - R_r^2$ $r_s^2 - R_r^2$ $r_s^2 - R_r^2$ $r_s^2 - R_r^2$	Depth FIRST	1116 SECOND 705.742 21.878 - 4.376 10.040	2'	Depth	112 SECOND 704.468 21.839 - 4.368 10.012	230' THIRE	<u>md. 1</u> cp md. 1 md. md. md.
Transmissibi Theoretical Flow Capaci Average Effective Permeability Indicated Flo Capacity Damage Rat Indicated	EQUA $EQUA$ $Frequence in the image is a constraint of the image is a c$	TION $p_r ZT$ $p_r ZT$ $p_r ZT$ $p_r ZT$ $p_r Z$ $p_r Z$	Depth FIRST	1116 SECOND 705.742 21.878 - 4.376 10.040 2.179	2'	Depth	112 SECOND 704.468 21.839 - 4.368 10.012 2.181	230' THIRE	md. 1 cp md. 1 md. 1 md. 1 md. 1 md. 1 MCF MCF
Transmissibi Theoretical Flow Capaci Average Effective Permeability Indicated Flo Capacity Damage Rat Indicated Flow Rate Theoretical	EQUA $EQUA$ $From Equation in the equation is the equation in the equation is the equation$	$\frac{ZT \log(0.472 \text{ b})}{2} \frac{ZT}{2}$ $\frac{ZT \log(0.472 \text{ b})}{2} \frac{ZT \log(0.472 \text{ b})}{2}$ $\frac{ZT \log(0.472 \text{ b})}{2} \frac{100 \text{ c}}{100 \text{ c}} \frac{100 \text{ c}}{100 \text{ c}}$ $\frac{100 \text{ c}}{100 \text{ c}} \frac{100 \text{ c}}{100 \text{ c}}$ $\frac{100 \text{ c}}{100 \text{ c}} \frac{100 \text{ c}}{100 \text{ c}}$	Depth FIRST	1116 SECOND 705.742 21.878 - 4.376 10.040 2.179 4442	2'	Depth	112 SECOND 704.468 21.839 - 4.368 10.012 2.181 4447	230' THIRE	md. 1 cp md. 1 md. md. md. f MCF MCF
Transmissibi Theoretical Flow Capaci Average Effective Permeability Indicated Fle Capacity Damage Rat Indicated Flow Rate	EQUA $Frequencies For the term of the term of the term of t$	TION $p_r ZT$ ZT Log(0.472 b) $r_s^2 - P_r^2$ $r_s^2 - P_r^2$ $r_s^2 - Ma$ $r_s^2 - Ma$ $r_s^2 - Ma$ $r_s^2 - Ma$ $r_s^2 - Ma$ $r_s^2 - Ma$ $r_s^2 - Ma$	Depth FIRST	1116 SECOND 705.742 21.878 4.376 10.040 2.179 4442 4307	2'	Depth	112 SECOND 704.468 21.839 - 4.368 10.012 2.181 4447 4309	230' THIRE	md. f rp md. f md. md. f md. f MCF MCF MCF
Transmissibi Theoretical Flow Capaci Average Effective Permeability Indicated Flo Capacity Damage Rat Indicated Flow Rate Theoretical Potential Ra Approx. Rad of	EQUA $EQUA$ $Frequence in the image is a constraint of the image is a c$	TION $p_r ZT$ ZT Log(0.472 b) $r_s^2 - P_r^2$ $r_s^2 - P_r^2$ $r_s^2 - Ma$ $r_s^2 - Ma$ r	Depth FIRST	1116 SECOND 705.742 21.878 - 4.376 10.040 2.179 4442 4307 9681	2'	Depth	112 SECOND 704.468 21.839 - 4.368 10.012 2.181 4447 4309 9699	230' THIRE	md. f rd. f md. f md. f md. f MCF MCF MCF
Transmissibi Theoretical Flow Capaci Average Effective Permeability Indicated Flo Capacity Damage Rat Indicated Flow Rate Theoretical Potential Ra Approx. Rad	EQUA $EQUA$ $Frequencies in the image in$	TION $p_r ZT$ zT Log(0.472 b) $r_s^2 - P_r^2$ $r_s^2 - P_r^2$ r_s^2 Ma r_s^2	Depth FIRST	1116 SECOND 705.742 21.878 - 4.376 10.040 2.179 4442 4307 9681	2'	Depth	112 SECOND 704.468 21.839 - 4.368 10.012 2.181 4447 4309 9699	230' THIRE	md. 1 cp md. 1 md. md. md. f MCF MCF MCF