

JUN 07 1983

c/sr
File

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test 4 pt. ☒ Initial ☐ Annual ☐ Special				Test Date 6-1-83		O. C. D. ARTESIA, OFFICE	
Conn. by W. A. MONCRIEF, JR. ✓				Connection EPNG			
Pool Undesignated				Formation Canyon Lime		Unit	
Completion Date 5-27-83		Total Depth 10,700		Plug Back TD 9039		Elevation 3993 G.L.	
Casing Size 4.5		Wt. 11.6		Set At 10,694		Perforations: From 8,972 To 8,987	
Tub. Size 2 3/8"		Wt. 4.7		Set At 8,930		Perforations: From open To ended	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single				Packer Set At 8,930		County Eddy	
Producing Thru Tbg.		Reservoir Temp. °F 163 @ 8930		Mean Annual Temp. °F 60		Baro. Press. - P _g 13.2	
8,930		H 8,930		C _g .690		% CO ₂ .20	
				% N ₂ .88		% H ₂ S 0	
				Prover		Meter Run 4.027	
						Taps Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Flow Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2196				24 hrs.
1.	4.0 X 1.250			694	1.44	91	2000		PKR		1 hr.
2.	4.0 X 1.250			713	4.0	90	1859		"		1 hr.
3.	4.0 X 1.250			731	9.0	89	1795		"		1 hr.
4.	4.0 X 1.250			745	16.0	82	1575		"		1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{spv}	Rate of Flow Q, Mcid
1	7.469	31.91	707.2	.9715	1.204	1.040	290
2	7.469	53.90	726.2	.9723	1.204	1.040	490
3	7.469	81.84	744.2	.9732	1.204	1.043	747
4	7.469	110.14	758.2	.9795	1.204	1.045	1,014
5.							

NO.	$\bar{\rho}_L$	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	14.603 Mcf/bbl.
1	1.06	551	1.63	.925	A.P.I. Gravity of Liquid Hydrocarbons	59 @ 60° Deg.
2	1.09	550	1.63	.924	Specific Gravity Separator Gas	.690
3	1.11	549	1.62	.920	Specific Gravity Flowing Fluid	X X X X X
4	1.13	542	1.60	.915	Critical Pressure	669 P.S.I.A.
5					Critical Temperature	238 R

NO.	P _c	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.095$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.095$
1	2209.2	2013.8	4055.4	825.2	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.125$	Post ID-2 6-17-83 Camp Canyon
2		1874.0	3511.9	1368.7		
3		1812.5	3285.3	1595.3		
4		1597.4	2551.8	2328.8		
5						

Absolute Open Flow		2,125 Mcid @ 15.025	Angle of Slope	45°	Slope, n	1.000
Remarks: Well made 7.25 bbls. of 59 @ 60° API Condensate.						

Approved By Division	Conducted By EL PASO EXPLORATION CO R. McMurray & B. Rea	Calculated By EL PASO EXPLORATION CO. R. McMurray & B. Rea	Checked By:
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