

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 1-9-82		JAN 25 1982	
Company Jake L. Hamon				Connection To Atmosphere					
Pool Carlsbad Morrow, South				Formation Morrow				Unit ARTESIA, OFFICE	
Completion Date 1-11-82		Total Depth 12,020		Plug Back TD 11,646		Elevation 3245.3 GR.		Farm or Lease Name St. "V" 249	
Casing Size 4 1/2" linear		Wt. 14.96		Set At 3.826		Perforations: From 11,546 To 11,602		Well No. 1	
Tub. Size 2 3/8"		Wt. 4.7#		Set At 1.995		Perforations: From OPEN ENDED		Unit Sec. Twp. Rge. M 36 23S 26 E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 11,470		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 173° 11,574'		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State N. Mex.	
L 11,574		H 11,574		G _g .5857		% CO ₂ 1.532		% N ₂ .289	
						% H ₂ S		Prover	
								Meter Run	
								Taps 4" Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3610		PKR	CHOKE	24 Hrs.
1.	4	x	1"	450	12"	76°	3365	38°		5/64	1 Hr.
2.	4	x	1"	450	23"	77	3151	43		6/64	1 Hr.
3.	4	x	1"	450	42"	80	2897	45		7.5/64	1 Hr.
4.	4	x	1"	450	58"	79	2606	53		9/64	1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.753	74.55	463.2	.9850	1.037	1.035	472
2	4.753	103.22	463.2	.9840	1.307	1.034	652
3	4.753	139.48	463.2	.9813	1.307	1.034	879
4	4.753	163.91	463.2	.9822	1.307	1.034	1034
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio TSTM	Mcft/bbl.
1	.69	536	1.52	.934	A.P.I. Gravity of Liquid Hydrocarbons	Deg.
2	.69	537	1.53	.936	Specific Gravity Separator Gas .5857	XXXXXXX
3	.69	540	1.53	.936	Specific Gravity Flowing Fluid XXXXX	
4	.69	539	1.53	.936	Critical Pressure 676. P.S.I.A.	P.S.I.A.
5					Critical Temperature 352. R	R

$P_r^2 = 3594.7$ $P_c^2 = 12,921.9$				$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 2.1661$	$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.575$
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	
1		3354.8	11254.7	1667.2	
2		3167.1	10030.5	2891.4	
3		2913.5	8488.5	4433.4	
4		2637.5	6956.4	5965.5	
5					

Absolute Open Flow 1,629 Mcfd @ 15.025			Angle of Slope 59° 33'	Slope, n .5879
Remarks: * Calculated from known Bottom Hole Pressures.				
Approved By Commission: Conducted By: M.R. Calculated By: M.K. Checked By: M.K.				