

N MEXICO OIL CONSERVATION COMM. JN
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 4-29-82		MAY 25 1982		
Company El Paso Natural Gas Co.				Connection El Paso Natural Gas Co.				O. C. D.	
Pool Baldridge Canyon				Formation Morrow				Unit ARTESIA, OFFICE	
Completion Date 3-8-82		Total Depth 10,933		Plug Back TD 10,854		Elevation 4032 GL		Farm or Lease Name Jurnegan St. Com.	
Csg. Size 4 1/2	Wt. 11.6	d 	Set At 10,933	Perforations: From 10,683 To 10,815				Well No. 2	
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 10,605	Perforations: From To				Unit Sec. Twp. Rye. G 12 24 24	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 10,605		County Eddy		
Producing Thru tbg		Reservoir Temp. °F 180 @ 10,605 (cal)		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico	
L 10,605	H 10,605	G _g .583	% CO ₂ 	% N ₂ 	% H ₂ S 	Prover 	Meter Run 4"	Taps Flg	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2202		Pkr		24 hrs
1.	4 X 1.000			555	9.84	112	2161		Pkr		30 min
2.	4 X 1.000			557	13.69	114	2121		Pkr		1 hr
3.	4 X 1.000			563	31.36	98	2062		Pkr		1 hr
4.	4 X 1.000			568	73.96	72	1932		Pkr		1 hr
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	4.753	52.44	568.2	.9535	1.310	1.034	322
2	4.753	88.35	570.2	.9518	1.310	1.034	541
3	4.753	134.42	576.2	.9653	1.310	1.035	836
4	4.753	207.32	581.2	.9887	1.310	1.045	1,334
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio ----- Mcf/bbl.
1.	.85	572	1.63	.935	A.P.I. Gravity of Liquid Hydrocarbons <u>dry gas</u> Deg.
2.	.85	574	1.64	.935	Specific Gravity Separator Gas <u>.583</u> X X X X X X X X
3.	.86	558	1.59	.934	Specific Gravity Flowing Fluid <u>X X X X X</u>
4.	.86	532	1.52	.915	Critical Pressure <u>672</u> P.S.I.A. P.S.I.A.
5.					Critical Temperature <u>350</u> R R

P _c 2215.2	P _c ² 4907.1	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.597$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.409$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		2175.6	4733.2	173.9
2		2137.0	4566.8	340.3
3		2080.9	4330.1	577.0
4		1959.5	3839.6	1067.5
5				

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.548$

4.548 Mcfd @ 15.025

Absolute Open Flow	4,548	Angle of Slope θ	51.25	Slope, n	.804
Remarks: No fluid made during test					
Approved By Commission:	Conducted By:	Calculated By:	Checked By:		
	Bill Rea & R. McGowen	J. B. Murray			