NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
AUG 30 1982
O. C. D.
ARTESIA, OFFICE

Type Test: [X] Initial FOUR POINT [ ] Annual [ ] Special			Test Date: 4-1-82	1980 FEL
Company: READ & STEVENS OIL CO.	Connection: AIR NEW WELL			810 FSL
Pool: UNDESIGNATED	Formation: MORROW			Unit: O
Completion Date: 4-1-82	Total Depth: 12,550	Plug Back TD: 12,500	Elevation:	Farm or Lease Name: CARRASCO
Csg. Size: 5.000 / Wt.: 23.0 / d: 4.154 / Set At: 12,500		Perforations: From 12,120 To 12,134		Well No.: 1
Tbg. Size: 2.375 / Wt.: 4.700 / d: 12,060 / Set At: 1.995		Perforations: From OPEN To ENDED		Unit: O / Sec.: 6 / Twp.: 23S / Rge.: 28E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE		Packer Set At: 8959		County: EDDY
Producing Thru: TUBING	Reservoir Temp. °F: 215 @ 12,127	Mean Annual Temp. °F: 60°	Baro. Press. – P_a: 13.2	State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
12,127	12,127	.573	1.153	.248			4.028	FLANGE

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	CHOKE	Duration of Flow
SI					2829				48 HRS
1.	4.028 X 1.500	400	2.0	86	2132	74		5/64	1
2.	4.028 X 1.500	400	6.0	78	1677	72		11/64	1
3.	4.028 X 1.500	400	12.0	81	1662	68		18/64	3/4
4.	4.028 X 1.500	400	20.0	70	1052	68		22/64	1
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.1200	28.75	413.2	.9759	1.3211	1.0260	423.
2	11.1200	49.79	413.2	.9831	1.3211	1.0281	739.
3	11.1200	70.42	413.2	.9804	1.3211	1.0271	1042.
4	11.1200	90.91	413.2	.9905	1.3211	1.0292	1361.
5							

NO.	P_t	Temp. °R	T_r	Z
1	.61	546	1.59	.590
2	.61	538	1.56	.946
3	.61	541	1.57	.948
4	.61	530	1.54	.944
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas .5730 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX .6078
Critical Pressure 678 P.S.I.A. _____ P.S.I.A.
Critical Temperature 344 R _____ R

P_c 3632.0 P_c^2 13191.4

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2813.9	7918.0	5273.0
2		2218.1	4920.0	8271.0
3		2208.5	4877.5	8314.0
4		1402.0	1965.6	11226.0
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1751$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1751$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1,599.3$

Absolute Open Flow 1,599.3 Mcfd @ 15.025 Angle of Slope θ .45 Slope, n 1.000

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	BENNETT-CATHEY	RICHARD TOWNLEY	