

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED 122

SEP 27 1982

4/5F

☒ Initial ☐ Annual ☐ Special				Test Date 9-21-82		O. C. D. ARTESIA OFFICE	
GULF EXPLORATION & PROD. ✓				Connection AIR			
WHITE CITY PENN				Formation ATOKA			
Completion Date 9-3-82		Total Depth 11646		Plug back TD 10710		Elevation 3449 G.L. WHITE CITY PENN	
Core Size 5"	Wt. 15	d	Set At 11646	Perforations: From 10068 To 10388		Well No. 2	
Trg. Size 2 3/8	Wt. n/80	d	Set At 10013	Perforations: From To		Unit Sec. Twp. Rge. K 29 24S 26 E	
Type well - Casing - Production - G.G. or G.O. Multiple SINGLE GAS				Packer Set At 10013		County EDDY	
Producing Time TBG.		Reservoir Temp. °F 174 @ 10013		Mean Annual Temp. °F 60°		State NEW MEXICO	
L 10013	H 10013	Gg .616	% CO ₂ .51	% N ₂ .68	% H ₂ S	Prover	Meter Run 4"
FLOW DATA				TUBING DATA		CASING DATA	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Duration of Flow
5.							
1.	4 x 1.500			610	4.0	108	72 HRS.
2.	4 x 1.500			615	11.0	90	1 HR.
3.	4 x 1.500			600	23.0	82	1 HR.
4.	4 x 1.500			615	59.0	94	1 HR.
5.							
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mgd
1.	10.84	49.93	623.2	.9568	1.274	1.042	687
2.	10.84	83.13	628.2	.9723	1.274	1.049	1171
3.	10.84	118.76	613.2	.9795	1.274	1.051	1688
4.	10.84	192.52	628.2	.9688	1.274	1.048	2699
5.							
NO.	R ₁	Temp. °R	T ₁	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas .616 XXXXXXXXXX Specific Gravity Flowing Fluid XXXXX Critical Pressure 671 P.S.I.A. P.S.I.A. Critical Temperature 365 °R °R		
1.	.93	568	1.56	.921			
2.	.94	550	1.51	.909			
3.	.91	542	1.48	.905			
4.	.94	554	1.52	.911			
5.							
$P_c = 4137.2$ $P_c^2 = 17116.4$					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 7.636$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.141$		
NO.	P ₁	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 7.636$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.141$		
1.		4059.7	16481.2	635.2			
2.		3968.7	15750.6	1365.8			
3.		3856.8	14874.9	2241.5			
4.		3646.7	13298.4	3818.0			
5.							
Absolute Open Flow 6,990 Mgd @ 15.025					Angle of Slope 55°		Slope, n .699
Remarks:							
Approved by Commission		Conducted By: DAVIS SERVICES, INC.		Calculated By: RICK PAGAN		Checked By:	

Post ID-2
10-8-82
Camp + BK