Form C-122
Revised 9-1-65

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

GSF File

Type Test: [X] Initial	[ ] Annual	[ ] Special
Test Date: 7-11-83		
Company: V.H. Westbrook	Connection: Air	
Pool: ~~South~~ Carlsbad	Formation: Wolfcamp	
Completion Date: 7-	Total Depth: 12030	Plug Back TD: ~~9700~~ 96
Elevation: ~~GL 3100~~ KB 3118	Farm or Lease Name: Grandi	Well No.: 1
Csg. Size: 5 1/2	Wt.: 17#	Set At: 12030
Perforations: From ~~9398~~ To ~~9624~~		
Tbg. Size: 2 7/8	Wt.: N/80	Set At: ~~9216~~
Perforations: From 96 To 96		
Unit: F	Sec.: 22	Twp.: 22S, Rge.: 27E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 9216	County: Eddy
Producing Thru: tbg	Reservoir Temp. °F: 170 @ 9572	Mean Annual Temp. °F:
Baro. Press. – P_a:	State: NM	
L: 9572	H: 9572	Gg: 0.6739
% CO_2: 0.445	% N_2: 0.881	% H_2S:
Prover:	Meter Run: 4.026	Taps: Flg

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI					4120		Pkr		48 hrs
1.	4 X 1.000	600	7.00	106	3540	75			1 hr
2.	4 X 1.000	640	11.00	112	2960	75			1 hr
3.	4 X 1.000	640	18.00	116	2540	75			1 hr
4.	4 X 1.000	650	44.00	112	1940	75			1 hr
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor F_t	Gravity Factor F_g	Super Compress. Factor, F_{pv}	Rate of Flow Q, Mcfd
1	4.753	65.52	613.2	.9585	1.218	1.052	382
2	4.753	84.71	653.2	.9535	1.218	1.052	492
3.	4.753	108.43	653.2	.9501	1.218	1.052	627
4.	4.753	170.82	663.2	.9535	1.218	1.052	992
5.							

NO.	P_r	Temp. °R	T_r	Z
1	.92	566	1.48	.904
2.	.98	572	1.50	.903
3.	.98	576	1.50	.903
4.	.99	572	1.51	.904
5.				

Gas Liquid Hydrocarbon Ratio ______ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ______ Deg.
Specific Gravity Separator Gas 0.6739 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 669 P.S.I.A. ______ P.S.I.A.
Critical Temperature 382 R ______ R

* P_c 4813.3 P_c^2 23,168.1

NO	BHP	P_w	P_w^2	$P_c^2 - P_w^2$
1	5300.2	4241.8	17993.1	5175.0
2	4734.2	3742.3	14005.0	9163.1
3	4176.2	3259.9	10626.9	12541.2
4	3586.2	2766.6	7654.3	15513.8
5	5930.2	SIP		

(1) $\frac{P_c^2}{P_c^2 - P_w^2}$ = 1.493

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 1.410

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 1,399

Post ID-2 7-12-83 Comp + BL

Absolute Open Flow 1,399 Mcfd @ 15.025

Angle of Slope θ 49.5 Slope, n .857

Remarks: * Calculated from B.H.P.
Pressures affected by fluid

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Davis Services, Inc.	J.D. Davis	