

RECEIVED

415r
File

☒ Initial FEB 01 1983 Annual		☐ Special		Test Date 1-24-83	
Company READ & STEVENS O. C. D.			Connection AIR NEW WELL		
Location ARTESIA, OFFICE UNDESIGNATED			Formation MORROW		
Completion Date 10-28-82		Total Depth 12764.		Plug Back TD 12350-12371	
Elevation 3083.		Form or Lease Name OGDEN		Well No. 12	
Size 5.500	Wt. 18.0	d 4.892	Set At 12350.	Perforations: From 12230. To 12338.	
Size 2.375	Wt. 4.7	d 1.995	Set At 11917.	Perforations: From 0 To 0	
Type Well - Single - Production - G.C. or G.O. Multiple				Depth of Set At 11917.	
SINGLE				EDDY	
Producing thru TUBING		Reservoir Temp. °F 195.0 12284.		Mean Annual Temp. °F 60.0	
L 12284.		H 12284.		Baro. Press. - P _a 13.2	
G _g 0.584		% CO ₂ 2.24		% N ₂ 0.	
% H ₂ S 0.		Prover 0.		Meter Run 4.0	
Taps FLANGE					

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1	4.03 X 0.750			445.	12.0	84.	3787.	65.			72.0
2	4.03 X 0.750			463.	36.0	76.	3713.	64.	0.	0.	1.0
3	4.03 X 0.750			473.	87.7	80.	3620.	67.	0.	0.	1.0
4	4.03 X 0.750			485.	48.0	55.	3352.	67.	0.	0.	1.0
5							3047.	63.	0.	0.	1.0

RATE OF FLOW CALCULATIONS							
NO	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super. Compress. Factor, F _{sp}	Rate of Flow Q, Mhd
1	2.66	74.15	458.2	0.9777	1.3086	1.0326	261.
2	2.66	130.93	476.2	0.9850	1.3086	1.0358	465.
3	2.66	206.55	486.2	0.9813	1.3086	1.0356	731.
4	4.75	154.64	498.2	1.0048	1.3086	1.0440	1009.
5							

NO	P _h	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.L. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.68	544.	1.54	0.938	0.	0.	0.584	X X X X X X X X	673.	354.
2	0.71	536.	1.52	0.932				X X X X X		
3	0.72	540.	1.53	0.933						
4	0.74	515.	1.46	0.917						
5										

NO	P _h	P _w	P _h ²	P _w ²	P _h ² - P _w ²
1	13885.	3724.	13868.	542.	
2	13200.	3629.	13166.	1244.	
3	11325.	3364.	11318.	3092.	
4	9365.	3071.	9430.	4980.	
5					

$$(1) \frac{P_h^2}{P_h^2 - P_w^2} = 2.8933$$

$$AOF = Q \left[\frac{P_h^2}{P_h^2 - P_w^2} \right]^n = 1928.$$

$$(2) \left[\frac{P_h^2}{P_h^2 - P_w^2} \right]^n = 1.9114$$

Post ID-2
2-4-83
Comp & BH

Estimated Open Flow 1928.	Mhd @ 15.025	Angle of Slope @ 58.6	Slope, n 0.610
------------------------------	--------------	-----------------------	----------------

Approved By Commission:	Conducted By: RICHARD TOWNLEY	Calculated By: BENNETT & CATHEY	Checked By:
-------------------------	----------------------------------	------------------------------------	-------------