

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR

Form C-122
Revised 9-1-65

RECEIVED

FEB 23 1983

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 2-14-83	
Company THE EASTLAND OIL CO. ✓		Connection AIR NEW WELL	
Pool UNDESIGNATED		Formation ATOKA	
Completion Date 2-9-83		Total Depth 13020.	
Plug Bar 12943.		Elevation 2975.	
Form or Lease Name FORTSON FED. COM.		Well No. 1	
Perforations: From 11875. To 11919.		Unit F 12 24S 28E	
Perforations: From 0. To 0.		County EDDY	
Type Well - Single - (Wardenhead - O.O. or G.O. Multiple) SINGLE		Packer Set At 10350.	
Producing thru TUBING		Baro. Press. - P _g 13.2	
State NEW MEXICO			
L 11897.	H 11897.	Q _g 0.584	% CO ₂ 0.73
		% N ₂ 1.47	% H ₂ S 0.
		Prover 0.	Meter Run 4.0
			Type FLANGE

FLOW DATA						TUBING DATA		B.H.P. DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. in. H ₂ O	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		CHOKE
SI							5957.	56.			113.5
1.	4.03 X 1.250			435.	7.0	56.	5465.	58.	0.	4/64	1.0
2.	4.03 X 1.250			445.	13.0	51.	5040.	60.	0.	5/64	1.0
3.	4.03 X 1.250			450.	25.0	46.	4328.	60.	0.	6.25/64	1.0
4.	4.03 X 1.250			455.	38.0	47.	3470.	61.	0.	9.5/64	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1	7.46	56.01	448.2	1.0039	1.3081	1.0370	569.
2	7.46	77.18	458.2	1.0088	1.3081	1.0394	789.
3	7.46	107.61	463.2	1.0137	1.3081	1.0414	1108.
4	7.46	133.39	468.2	1.0127	1.3081	1.0416	1372.
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NO.	P ₁	Temp. °R	T ₁	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.67	516.	1.48	0.930	0.	0.	0.584	XXXXXX	674.	348.
2	0.68	511.	1.47	0.926						
3	0.69	506.	1.45	0.922						
4	0.69	507.	1.46	0.922						
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NO.	P ₁ ²	P _w	R _w ²	P _c ² - R _w ²
1	30011.	5485.	30086.	5658.
2	25535.	5058.	25588.	10156.
3	18846.	4348.	18909.	16835.
4	12133.	3492.	12191.	23553.
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(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.5176$ (2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.2937$

AOF = 0 $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1775.$

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