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NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 8-22-85

Company: DINERO OPERATING COMPANY	Connection: EL PASO NAT		
Pool: DUBLIN RANCH	Formation: MORROW		Unit: P
Completion Date: 8-21-85	Total Depth: 12517'	Plug Back TD: 12517'	Elevation: 3077'
Farm or Lease Name: DINERO STATE			
Csg. Size: 5.000 / Wt.: 23.0 / d: 4.044 / Set At: 12517'	Perforations: From 12308' To 12436'		Well No.: 2
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995 / Set At: 12052	Perforations: From 0 To 0		Unit: P / Sec.: 16 / Twp.: 22S / Rge.: 28E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE	Packer Set At: 11074'		County: EDDY
Producing Thru: TUBING	Reservoir Temp. °F: 192 @ 12374'	Mean Annual Temp. °F: 60.0	Baro. Press. – P_a:	State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
12374'	12374'	0.580	1.08	0.16	0	0	4.0	FLANGE

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					2281	91			24.5
1.	4.03 X 1.000	312	0.8	98	1968	91			1.0
2.	4.03 X 1.000	312	2.6	100	1690	86			1.0
3.	4.03 X 1.000	314	4.0	94	1220	84			1.0
4.	4.03 X 1.000	314	5.3	94	875	83			1.0
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.75	16.22	324.9	0.9653	1.3133	1.0200	100
2	4.75	28.84	324.9	0.9636	1.3133	1.0197	177
3	4.75	36.18	327.2	0.9688	1.3133	1.0208	223
4.	4.75	41.60	327.2	0.9688	1.3133	1.0208	257
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	0.48	558	1.59	0.961
2.	0.48	560	1.60	0.962
3.	0.48	554	1.58	0.960
4.	0.48	554	1.58	0.960
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: 0 Deg.

Specific Gravity Separator Gas	0.580	XXXXXXXXX
Specific Gravity Flowing Fluid	XXXXX	0.580
Critical Pressure	678 P.S.I.A.	678 P.S.I.A.
Critical Temperature	350 R	350 R

P_c 2264.0 P_c^2 1526

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		1956	3825	1301
2		1686	2843	2283
3		1223	1496	3630
4		883	779	4347
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1793$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1375$

Post ID-2
9-27-85
Comp + BK

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 292$

Absolute Open Flow: 292 Mcfd @ 15.025 — Angle of Slope θ: 52.0 — Slope, n: 0.781

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	BENNETT & CATHEY	RICHARD TOWNLEY	