NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

4SF File

RECEIVED
APR 17 1985

Type Test ☒ Initial	☐ Annual	☐ Special			Test Date 4-12-85	
Company POGO PRODUCING		Connection TO AIR				
Pool Malaga Morrow		Formation MORROW				Unit
Completion Date 4-11-85	Total Depth 12820	Plug Back TD 12791		Elevation 0		Farm or Lease Name LIGHTFOOT COM
Csg. Size 5.000	Wt. 18.0	d 4.276	Set At 12797	Perforations: From 12709	To 12766	Well No. 2
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 12638	Perforations: From 0	To 0	Unit P Sec. 14 Twp. 24S Rge. 28E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple SINGLE			Packer Set At 12638			County EDDY
Producing Thru TUBING	Reservoir Temp. °F 190@ 12728	Mean Annual Temp. °F 12760.0	Baro. Press. – P_a 13.2			State NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
12728	12728	0.580	0.98	0.37	0	0	4.0	FLANGE

	FLOW DATA						TUBING DATA		B.H.P. DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	CHOKE	
SI							4162		5541	3/64	23.2
1.	4.03	X	1.750	520	4.0	120	3355	0	4839	3/64	1.0
2.	4.03	X	1.750	560	5.0	110	3050	0	4490	6/64	1.0
3.	4.03	X	1.750	560	9.0	81	2287	0	3531	8/64	1.0
4.	4.03	X	1.750	565	12.0	67	1580	0	2536	10/64	1.0
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	14.93	46.18	533.2	0.9469	1.3131	1.0274	881
2	14.93	53.54	573.2	0.9551	1.3131	1.0317	1034
3	14.93	71.82	573.2	0.9804	1.3131	1.0396	1435
4	14.93	83.30	578.2	0.9933	1.3131	1.0442	1693
5							

NO.	P_r	Temp. °R	T_r	Z
1	0.79	580	1.66	0.947
2	0.85	570	1.63	0.939
3	0.85	541	1.55	0.925
4	0.85	527	1.51	0.917
5				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 0 Deg.
Specific Gravity Separator Gas 0.580 | X X X X X X X X X
Specific Gravity Flowing Fluid X X X X X | 0.580
Critical Pressure 677 P.S.I.A. | 677 P.S.I.A.
Critical Temperature 350 R | 350 R

P_c 4350.3 P_c^2 18925

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	23544	3750	14065	4860
2	20279	3459	11962	6963
3	12561	2683	7200	11725
4	6498	1923	3699	15226
5				

$$(1)\ \frac{P_c^2}{P_c^2 - P_w^2} = 1.2429 \qquad (2)\ \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1411$$

$$\text{AOF} = Q\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1931.8$$

Post ID-2
4-26-85
Comp & PK

Absolute Open Flow 1932 Mcfd @ 15.025 | Angle of Slope θ 58.75 | Slope, n .607

Remarks:

Approved By Commission:	Conducted By: Bennett & Cathey	Calculated By: Richard Townley	Checked By: