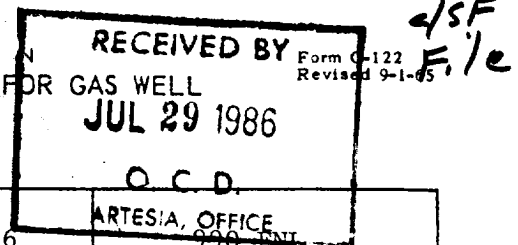


NE MEXICO OIL CONSERVATION COMMS
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL



Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7-14-86		O.C.D. ARTESIA, OFFICE	
Company TXO PRODUCTION CO. ✓				Connection CABOT GP&P		1980 FEL	
Pool East Carlsbad <i>Wolfcamp</i>				Formation Wolfcamp		Unit B	
Completion Date 6-24-86		Total Depth 10,700'		Plug Back TD 10,656'		Elevation 3110 KB 3082 Gr.	
Csg. Size 4 1/2"		Wt. 11.6		Set At 4.000		Perforations: From 9707 To 9857	
Tbg. Size 2 3/8"		Wt. 4.7		Set At 1.995		Perforations: From OPEN-ENDED	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 9590'		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 188° @ 9782'		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2	
L 9782		H 9782		Gg .677		% CO ₂ 1.21	
				% N ₂ .701		% H ₂ S	
				Prover		Meter Run 3"	
						Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							2584		PKR	CHOKE	24 Hrs.
1.	3	X	1.000	681	7.29	81°	2298			6/64	1 Hr.
2.	3	X	1.000	689	15.21	94	2101			8/64	1 Hr.
3.	3	X	1.000	691	23.04	99	1831			10/64	1 Hr.
4.	3	X	1.000	699	42.25	94	1600			12/64	1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	4.789	71.14	694.2	.9804	1.215	1.072	435
2	4.789	103.35	702.2	.9688	1.215	1.063	619
3	4.789	127.38	704.2	.9645	1.215	1.062	759
4	4.789	173.47	712.2	.9688	1.215	1.064	1041
5							

NO.	R _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	1.04	541	1.42	.870	9.9	55.1 @ 60°	.677	X X X X X X X X	669	382
2	1.05	554	1.45	.885				X X X X X		
3	1.05	559	1.46	.886					P.S.I.A.	P.S.I.A.
4	1.06	554	1.45	.884					R	R
5										

* P_c 2783.6 P_c² 7748.4

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	3617.2	2632.4	6929.5	818.9
2	3433.2	2469.3	6097.3	1651.1
3	3229.2	2206.2	4867.3	2881.1
4	2895.2	1882.3	3543.2	4205.2
5	2470.2			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.843$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.385$

AGF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.442$

Absolute Open Flow	1.442	Mcfd @ 15.025	Angle of Slope θ	62°	Slope, n	.533
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Remarks: Made 12.00' bbls. condensate during test. 56.6 @ 74°, Test calculated from known BHP'S

* = Static BHP Converted back to surface. ** = BHP'S.

Approved By Commission:	Conducted By: W.S.	Calculated By: B.M.	Checked By: B.M.
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