

JUN 24 1986

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL
O. C. D.

Type Test:		☒ Initial		☐ Annual		☐ Special		Test Date		ARTESIA, OFFICE	
Company				Connection							
Union Oil Company of California				None							
Pool				Formation				Unit			
Wildcat Morrow Pool				Morrow							
Completion Date		Total Depth		Plug Back TD		Elevation		Farm or Lease Name			
5/4/86		15136		14550		3459		Barclay State			
Coq. Size	Wt.	d	Set At	Perforations:				Well No.			
4 1/2"	13.5	4.5	15133	From 14062		To 14466		1			
Thq. Size	Wt.	d	Set At	Perforations:				Unit Sec. Twp. Rye.			
2"	4.7	2.375	12275	From		To		I 2 23S 31E			
Type Well - Single - Bradenhead - G.C. or G.O. Multiple						Packer Set At		County			
Single						12275		Eddy			
Producing Thru tubing		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _g		State			
		167 @ 14062'		60		13.2		New Mexico			
L	H	G _g	% CO ₂	% N ₂	% H ₂ S	Prover.	Meter Run	Taps			
14062	14062	0.598	0	0	0	0	2.9	Flange			

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							5000	65			68.5
1.	2.9		0.500	640	3.5	97	4720	99	0	0	1
2.	2.9		0.500	670	13.5	93	4540	98	0	0	0.7
3.	2.9		0.500	650	34.0	90	4240	95	0	0	0.7
4.	2.9		0.500	630	76.0	82	3640	88	0	0	0.7
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	1.18	47.81	653.2	0.9662	1.2932	1.0444	74
2	1.18	96.04	683.2	0.9697	1.2932	1.0479	149
3	1.18	150.16	663.2	0.9723	1.2932	1.0475	234
4	1.18	221.10	643.2	0.9795	1.2932	1.0488	348
5.							

NO.	R _g	Temp. °R	T _g	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.97	557	1.56	0.917	0	0	0.598	X X X X X X X X	673	358
2.	1.02	553	1.55	0.911						
3.	0.99	550	1.54	0.911						
4.	0.96	542	1.51	0.909						
5										

P _c 5010.6		P _c ² 25106		(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.0804$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.9959$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²			
1		4673	21840	3266			
2		4494	20199	4908			
3		4199	17629	7478			
4		3611	13038	12068			
5							

Absolute Open Flow 694 Mcfd @ 15.025 Angle of Slope 46.7 Slope, n 0.943

Remarks:

Approved By Division Conducted By: Correlated By: Checked By:

C. A. Beal M. E. G. 110

clsf File

Post #0-2
7-12-86
Comp & BK