

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 2/15/89		MAR 07 '89	
Company R. E. HIBBERT		Connection AIR			
Pool <i>Monterey Canyon Strawn</i>		Formation STRAWN		Unit O. C. D.	
Completion Date 2/4/89		Total Depth 10068		Plug Back TD 10058	
Elevation 0		Form or Lease Name RIDGE STATE		Well No. 1	
Cq. Size 4.500	Wt. 11.6	d 4.000	Set At 10068	Perforations: From 10030 To 10040	
Tq. Size 2.375	Wt. 4.7	d 1.995	Set At 9986	Perforations: From 0 To 0	
Type Well - Single - Dradhead - G.C. or G.O. Multiple SINGLE-GAS				Packer Set At 9986	
Producing Thru TUBING		Reservoir Temp. °F 175 @ 10035		Mean Annual Temp. °F 60	
L 10035		H 10035		Baro. Press. - P _a 13.2	
Cq .632		% CO ₂ .21		% N ₂ .01	
% H ₂ S .00		Prover .0		Meter Run 4.0	
Taps FLANGE		County EDDY		State NEW MEXICO	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	4.03 X 1.250			500	2.0	70	1917	60			72.0
2.	4.03 X 1.250			500	2.0	70	1420	60	0	0	1.0
3.	4.03 X 1.250			500	2.0	70	972	60	0	0	1.0
4.	4.03 X 1.250			500	2.0	70	972	60	0	0	1.0
5.							972	60	0	0	1.0

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor F _{sp}	Rate of Flow Q, Mcfd
1.	7.47	32.04	513.2	.9905	1.2579	1.0472	312
2.	7.47	32.04	513.2	.9905	1.2579	1.0472	312
3.	7.47	32.04	513.2	.9905	1.2579	1.0472	312
4.	7.47	32.04	513.2	.9905	1.2579	1.0472	312
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.76	530.	1.44	.912	0	0	.632	XXXXXX	672.	368.
2.	.76	530.	1.44	.912						
3.	.76	530.	1.44	.912						
4.	.76	530.	1.44	.912						
5.										

NO.	P _r ²	P _w	P _w ²	P _r ² - P _w ²
1.	2054.	1435.	2060.	1666.
2.	971.	987.	975.	2751.
3.	971.	987.	975.	2751.
4.	971.	987.	975.	2751.
5.				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3544$

AOF = Q $\left[\frac{P_r^2}{P_c^2 - P_w^2} \right]^n = 423.$

(2) $\left[\frac{P_r^2}{P_c^2 - P_w^2} \right]^n = 1.3544$

*Post ID-2
3-10-89
comp & RK*

Absolute Open Flow 423.		Mcf/d @ 15.025	Angle of Slope @ 45.0	Slope, n 1.000
Remarks: 1ST RATE 4/64 2ND RATE 6/64				

Approved By Division	Conducted By: BENNETT & CATHEY	Calculated By: MATT LEE	Checked By:
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