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JUL 17 '89

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLForm C-122
Revised 9-1-65O. C. D.
AREA OFFICE

☒ Initial		☐ Annual		☐ Special		Test Date 6-28-89	
Company W.A. Moncrief Jr. ✓				Connection			
Pool Undesignated <i>Wilcox Penn</i>				Formation Upper Penn		Unit Robinia Draw WI Unit	
Completion Date 6-28-89		Total Depth 10,830		Plug Back TD 8515		Elevation 4122GL	
Csg. Size 5 1/2"		Wt. 17#		Set At 4.767		Perforations: From 8402 To 8412	
Tbg. Size 2 7/8"		Wt. 6.5		Set At 2.441		Perforations: From To	
Type Well - Single - Broadhead - G.G. or G.O. Multiple Single				Packer Set At 8326		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 151 @ 8402		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.20	
L 8402		H 8326		Gg 0.7092		% CO ₂ 0.29	
				% N ₂ 1.33		% H ₂ S 0	
				Prover		Meter Run 4"	
						Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
51							2985	80			72
1.	4.026	x	1.250	300	14	70	2936	85			1
2.	4.026	x	1.250	300	41	77	2865	85			1
3.	4.026	x	1.750	300	38	60	2582	85			1
4.	4.026	x	1.750	300	80	49	2175	85			1
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _L	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	7.47	66.22	313.2	0.9905	1.875	1.0352	602
2	7.47	113.32	313.2	0.9840	1.875	1.0334	1022
3	14.93	109.09	313.2	1.0000	1.875	1.0377	2007
4	14.93	158.29	313.2	1.0107	1.875	1.0401	2949
5.							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.47	530	1.36	0.933	14.4	58.9	0.709	X X X X X X X X	666	389
2	0.47	537	1.38	0.936				X X X X X		
3	0.47	520	1.34	0.929						
4	0.47	509	1.31	0.924						
5										

NO.	P _f	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1		3988	15904	1205.5	2.1885	2.1885
2		3894	15163	1943.5		
3		3549	12595	4511.5		
4		3048	9290	7816.5		
5						

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6459$$

Part ID-2
7-28-89
comp & BK

Absolute Open Flow 6459 Mcfd @ 15.015 Angle of Slope θ 45° Slope, n 1.000

Remarks:

Approved By Commission: Conducted By: Calculated By: Checked By: