

cls
File

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 1/8/90		ARTESIA, CHANCE	
Company Santa Fe Energy ✓		Connection Pipeline			
Pool <u>Salt Draw Atoka Gas</u> Undesignated		Formation Atoka		Unit	
Completion Date 12/9/89		Total Depth 13450		Plug Back TD 12520	
		Elevation 0		Farm or Lease Name Salt Draw 28 <i>Fed.</i>	
Coq. Size 5.500	Wt. 23.0	d 4.670	Set At 13450	Perforations: From 11660 To 11667	
Thq. Size 2.375	Wt. 4.7	d 1.995	Set At 14493	Perforations: From 0 To 0	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single-Gas				Packer Set At 11457	
Producing Thru Tubing		Reservoir Temp. °F 188 @ 11664		Mean Annual Temp. °F 60.0	
		Baro. Press. - P _g 13.2		State NM	
L 11664	H 11664	G _g .588	% CO ₂ .46	% N ₂ .56	% H ₂ S .00
Prover .0		Meter Run 2.1		Taps Flange	

FLOW DATA					TUBING DATA		BHP DATA		Duration of Flow	
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI								7920	188	72.0
1.	2.07 x 1.500		710	1.8	95	0	0	7428	188	1.0
2.	2.07 x 1.500		710	3.0	94	0	0	7102	188	1.0
3.	2.07 x 1.500		715	6.3	90	0	0	6354	188	1.0
4.	2.07 x 1.500		718	10.5	92	0	0	5216	188	1.0
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1	12.76	35.58	723.2	.9680	1.3041	1.0467	600.
2	12.76	46.58	723.2	.9688	1.3041	1.0471	786.
3	12.76	67.46	728.2	.9723	1.3041	1.0488	1145.
4	12.76	87.62	731.2	.9706	1.3041	1.0483	1483.
5							

NO.	P _g	Temp. °R	T _g	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	1.07	555	1.57	.913	0	0	.588	XXXXXX	674.	352.
2	1.07	554	1.57	.912						
3	1.08	550	1.56	.909						
4	1.08	552	1.57	.910						
5										

NO.	P _i	P _w	P _w ²	P _i ² - P _w ²
1	55371	6122	37476	5771
2	50626	5823	33912	9335
3	40541	5146	26480	16768
4	27345	4139	17135	26113
5				

(1) $\frac{P_i^2}{P_i^2 - P_w^2} = 1.6562$ (2) $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 1.3874$

AOR = 0 $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 2058.$

Absolute Open Flow	2058	Mcf @ 15.025	Angle of Slope θ	57.5	Slope, n	.637
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Remarks: Choke size: 1st rate 3.5/64 2nd rate 5/64
3rd rate 6/64 4th rate 7.5/64

Approved By Division	Conducted By Bennett & Cathey	Calculated By: Matt Lee	Checked By:
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