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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MARALO, INC.					Lease or Unit Name COCHITI FEDERAL COM. 5				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 7-25-95				
Completion Date 6-23-95		Total Depth 12200		Plug Back TD 11825		Elevation		Well No. 1	
Csg. Size 4 1/2		Wt. 15.1		Set At 12200		Perforations: From: 11460 To: 11568		Unit Ltr. - Sec. - TWP - Rge. 5-24S-29E	
Tbg. Size 2-7/8		Wt. 6.5		Set At 11192		Perforations: From: To:		County EDDY	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple					Packer Set At 11200			Formation WOLFCAMP	
Producing Thru TBG		Reservoir Temp. °F 18515 @ 11147		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection SALES LINE	
L *11147	H 11147	Gg .655	% CO ₂ .65	% N ₂ .28	% H ₂ S	Prover		Meter Run 3.068	Taps FLG

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice X Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						4090		PKR		12 hr.
1.	3 X 1.500		345	9.00	112	3960		"		1 hr.
2.	3 X 1.500		355	20.00	117	3760		"		1 hr.
3.	3 X 1.500		360	34.00	116	3530		"		1 hr.
4.	3 X 1.500		380	55.00	106	3225		"		1 hr.
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	11.13	56.78	358.2	.9535	1.236	1.028	765
2.	11.13	85.81	368.2	.9493	1.236	1.029	1153
3.	11.13	112.64	373.2	.9501	1.236	1.029	1517
4.	11.13	147.05	393.2	.9585	1.236	1.031	1999
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio DRY GAS Mcf/bbl.		
1.	.53	572	1.52	.946	A.P. I. Gravity of Liquid Hydrocarbons DRY	Deg.	
2.	.54	577	1.53	.945	Specific Gravity Separator Gas .655	XXXXXXXXXX	
3.	.55	576	1.53	.945	Specific Gravity Flowing Fluid	XXXXXX	
4.	.58	566	1.50	.941	Critical Pressure 670	P.S.I.A.	P.S.I.A.
5.					Critical Temperature 375	R	R

* _c 4143.8 p _c ² 17171.1					1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.244$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.207$				
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.412$				
1.	**	3996.7	15973.6	1197.5					
2.	**	3847.1	14800.2	2370.9					
3.	**	3675.8	13511.5	3659.6					
4.	**	3446.6	11879.1	5292.0					
5.									

Absolute Open Flow **4,412** Mcfd @ 15.025 Angle of Slope Θ **56.1** Slope, n **.6726**

Remarks: ***=BHP INSTRUMENT SET @ THIS DEPTH**
**** TEST CALCULATED FROM KNOWN BHP'S**

Approved By Division	Conducted By: PRO WELL TESTER	Calculated By: MB	Checked By: BM
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