BASS ENTERPRISES

Operator: BASS ENTERPRISES	Well Name: JRU #70
Project ID:	Location: EDDY CO,. NM

Design Parameters:

Mud weight (10.00 ppg): 0.519 psi/ft
Shut in surface pressure : 5602 psi
Internal gradient (burst) : 0.122 psi/ft
Annular gradient (burst) : 0.494 psi/ft
Tensile load is determined using buoyed weight
Service rating is "Sweet"

Design Factors:

Collapse : 1.000
Burst : 1.25
8 Round : 1.60 (J)
Buttress : 1.60 (J)
Other : 1.60 (J)
Body Yield : 1.60 (B)

	Length (feet)	Size (in.)	Weight (lb/ft)	Grade	Joint	Depth (feet)	Drift (in.)	Cost
1	2,400	5.500	17.00	S-95	VAM FJL	14,100	4.767	

	Collapse Load (psi)	Collapse Strgth (psi)	Collapse S.F.	Burst Load (psi)	Min Int Yield Strgth (psi)	Burst S.F.	Tension Load (kips)	Tension Strgth (kips)	Tension S.F.
1	7325	8580	1.171	5298	9190	1.73	35.19	267	7.59 J

Prepared by : *BJL, Midland, TX*
Date : 05-23-1994
Remarks :

Minimum segment length for the 14,100 foot well is 1,000 feet.
SICP is based on the ideal gas law, a gas gravity of 0.65, and a mean gas temperature of 145°F (Surface 74°F , BHT 215°F & temp. gradient 1.000°/100 ft.)
The liner string design has a specified top of 11,700 feet, and the choice of connection is VAM.
The burst load shown is the pressure at the top of the segment.
For burst purposes, tubing is considered to be set in a packer at 11,800 ft. using packer fluid weighing 9.000 ppg. The fluid behind the casing weighs 9.500 ppg and the load at the packer is 5,296 psi.
Pore and load pressures at TVD are 7,325 and 366 psi, respectively.
Buoyancy is determined using packer fluid.
An annular mud weight of 9.500 ppg was used for burst purposes. The differential mud gradient below any lost-circulation depth is -0.371 psi/ft and the bottom hole pressure load is 366 psi.

NOTE: The design factors used in this casing string design are as shown above. As a general guideline, Lone Star Steel recommends using minimum design factors of 1.125 - Collapse (with evacuated casing), 1.0 - Burst, 1.8 - 8 Round Tension, 1.6 - Buttress Tension, and 1.5 - Body Yield. Collapse strength under axial tension was calculated based on the Westcott, Dunlop and Kemler curve. Engineering responsibility for use of this design will be that of the purchaser.

Costs for this design are based on a 1987 pricing model. (Version 1.06)