(lune 1990) DEPARTME	TED, STATES IN.M. ON CONS. DA C HE INTERIOR 811 S. 1st Stre AND MANAGEMEN Artesia, NM 88210-2	0151-
Do not use this form for proposals to drill or	AND REPORTS ON WELLS to deepen or reentry to a different reservoir. R PERMIT—" for such proposals	 5. Lease Designation and Serial No. NM-0404441 6. If Indian, Allottee or Tribe Name
SUBMIT 1. Type of Well Oil Well Other 2. Name of Operator DEVON ENERGY PRODUCTION COMPA 3. Address and Telephone No. 20 NORTH BROADWAY, SUITE 1500, OK 4. Location of Well (Footage. Sec., T., R., M., or Survey I 1980' FNL & 1980' FEL, Section 13-23S-311	(LAHOMA CITY, OKLAHOMA 73102 (405) 235-3611 (405) 255-3611 (405) 255-3611 (405) 2	 7. If Unit or CA, Agreement Designation 8. Well Name and No. 7. Todd "13G" Federal #21 9. API Well No. 30-015- 10. Field and Pool, or Exploratory Area Sand Dunes (Delaware) 11. County or Parish, State Eddy County, NM
CHECK APPROPRIATE BOX(s TYPE OF SUBMISSION Notice of Intent Subsequent Report Final Abandonment Notice) TO INDICATE NATURE OF NOTICE, REPO TYPE OF ACTION	ORT, OR OTHER DATA Change of Plans New Construction Non-Routine Fracturing Water Shut-Off Conversion to Injection Dispose Water (Note: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)
12 Describe Proposed or Completed Operations (Clearly state all	pertinent details, and give pertinent dates, including estimated date of starting	any proposed work. If well is directionally drilled, give

Describe Proposed or Completed Operations (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work. If well is directionally drifted, give subsurface locations and measured and true vertical depths for all markers and zones pertinent to this work.)*

The original Application for Permit to Drill, Form 3160-3, was approved on 12/05/00 for a proposed depth of 6400' in the Cherry Canyon formation. Devon Energy Production Company, L.P. requests to amend the depth to 8750' in the Delaware Bone Springs formation.

0 - 4400' 8 5/8" 32# J55 LT&C - Cmt to surface

0 – 900' 5 ½" 17# J55 LT&C

900' - 7300' 5 ½" 15.5# J55 LT&C

7300' - 8750' 5 ½" 17# J55 LT&C

Cmt 5 $\frac{1}{2}$ " in 2 stages. 1 stage 620 sx/ Class H. Stage collar @ 5,500'. Cmt stage 2 w/370 sx Class C. The cement volumes could be revised pending the caliper measurement from the open hole logs. The top of cement is designed to reach 100' above the base of the 8 5/8" csg.

Please see the attached casing design for design conditions.

14. I hereby certify that the foregoing is true and correct				
		Karen A. Cottom		
Signed Min attom	Title	Engineering Technician	Date	June 19, 2001
(This space for Federal or State office use)				
(ORIG. SGD.) ALEXIS C. SWOBODA	Title	PETROLEUM ENGINEER	Date	JUN 21 2001
	Title_		Date	
Conditions of approval, if any:				

Title 18 U.S.C. Section 1001, makes it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations to any matter within its jurisdiction.



2001 JUN 21 AM 8: 40



Well nai Operato String ty	or: Dev		Production	-	Todd Federal any, L.P.								
Location	n: T23	S-R31E, Eo	dy County,	NM				<u>.</u>					
Collaps Mud V	weight:		9.000 ppg ed pipe.	Minimum design factors:Collapse: Design factor1.125Burst: Design factor1.00Eurst: Design factor1.00Tension: 8 Round STC:1.80 (J) 8 Round LTC:8 Round LTC:1.80 (J) 9 Buttress:9 Buttress:1.60 (J) 9 Premium:9 Dody yield:1.60 (B)Tension is based on air weight. Neutral point:738 ft		Environment: H2S considered? Surface temperature: Bottom hole temperature: Temperature gradient: Minimum section length:		No 75 °F 87 °F 1.40 °F/100ft 850 ft					
pro Interr Calcu	anticipated essure: hal gradient ulated BHP ackup mud	: 0 1	765 psi .335 psi/ft ,050 psi			1.80 (J) 1.80 (J) 1.60 (J) 1.50 (J) 1.60 (B)	Minimum section length: Non-directional string. Re subsequent strings: Next setting depth: Next mud weight: Next setting BHP: Fracture mud wt:		ngs: h: 4,400 ft : 9.800 ppg : 2,240 psi				
Run Seq 1	Segment Length (ft) 850	Size (in) 13.375	Nominal Weight (Ibs/ft) 48.00	Grade H-40	End Finish ST&C	True Vert Depth (ft) 850	Injection Measured Depth (ft) 850	Drift Diameter (in) 12.59	4,400 psi Est. Cost (\$) 10541				
Run Seq 1	Collapse Load (psi) 397	Collapse Strength (psi) 740	Collapse Design Factor 1.86	Burst Load (psi) 1050	Burst Strength (psi) 1730	Burst Design Factor 1.65	Tension Load (kips) 40.8	Tension Strength (kips) 322	Tension Design Factor 7.89 J				

Devon Energy

Date: June 19,2001 Oklahoma City, Oklahoma

Remarks: Collapse is based on a vertical depth of 850 ft, a mud weight of 9 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Engineering responsibility for use of this design will be that of the purchaser.



Well nar Operato String ty	r: Devo	n Energy nediate	Production		dd Fede L.P.	ral								
Location	n: T23S	-R31E, E	ddy County, N	M				<u> </u>						
Collaps Mud	paramete i <u>e</u> weight: nal fluid dens	1	0.000 ppg 0.200 ppg	Collapse: Design factor 1.125		Environment: H2S considered? Surface temperature: Bottom hole temperature: Temperature gradient:		No 75 °F 137 °F 1.40 °F/100ft						
				<u>Burst:</u> Design fac	tor	1.00	Minimum see		850 ft					
pr Inter Calc	anticipated s essure: nal gradient: ulated BHP ackup mud s	(1,882 psi).248 psi/ft 2,971 psi	<u>Tension:</u> 8 Round S 8 Round L Buttress: Premium: Body yield	TC:	1.80 (J) 1.80 (J) 1.60 (J) 1.50 (J) 1.60 (B)	Non-directional string. Re subsequent strings: Next setting depth: 8,8		8,800 ft					
				Tension is based on air weight. Neutral point: 3,747 ft		Next mud weight: 9.000 Next setting BHP: 4,114 Fracture mud wt: 13.000 Fracture depth: 4,400		9.000 ppg 4,114 psi 13.000 ppg 4,400 ft 2,971 psi						
Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (Ibs/ft) 32.00	Grade	End Finish LT&C	True Vert Depth (ft) 4400	Measured Depth (ft) 4400	Drift Diameter (in) 7.875	Est. Cost (\$) 35458					
1 Run Seq 1	4400 Collapse Load (psi) 2240	8.625 Collapse Strength (psi) 2530	Collapse	Burst Load (psi) 2971	Burst Strength (psi) 3930	Burst	Tension Load (kips) 140.8	Tension Strength (kips) 417	Tension Design Factor 2.96 J					

Devon Energy

Date: June 19,2001 Oklahoma City, Oklahoma

Remarks: Collapse is based on a vertical depth of 4400 ft, a mud weight of 10 ppg An internal gradient of .01 psi/ft was used for collapse from TD to Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Engineering responsibility for use of this design will be that of the purchaser.

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Max anticipated surface pressure: 3,216 psi Internal gradient: 0.100 psi/ft Tension: Non-directional string. Calculated BHP 4,091 psi 8 Round STC: 1.80 (J) No backup mud specified. Buttress: 1.60 (J) Premium: 1.50 (J) Body yield: 1.60 (B) Tension is based on air weight. Neutral point: 7,635 ft Testimated cost: 31,703 (\$) Run Segment Nominal End True Vert Measured Drift Seq Length Size Weight Grade Finish Depth Depth Diameter (ft) (in) (lbs/ft) J-55 LT&C 900 900 4.767				rai	odd Fede , L.P.		/ Productio	on Energy duction	tor: Dev	Well n Opera String	
Collapse Mud weight:9.000 ppg Design is based on evacuated pipe.Collapse: Design factorH2S considered? Surface temperature: Bottom hole temperatur Temperature gradient: Max anticipated surface pressure:H2S considered? Surface temperature: Bottom hole temperatur Temperature gradient: Max anticipated BHPMax anticipated surface 						NM	ddy County,	S-R31E, E	on: T23	Locatio	
Burst: Design factor 1.00 Burst: Design factor 1.00 Burst: Design factor 1.00 Max anticipated surface pressure: 3,216 psi Internal gradient: 0.100 psi/ft Tension: Non-directional string. Calculated BHP 4,091 psi 8 Round STC: 1.80 (J) No backup mud specified. Buttress: 1.60 (J) Premium: 1.50 (J) Body yield: 1.60 (B) Tension is based on air weight. Neutral point: 7,635 ft Estimated cost: 31,703 (\$) Depth Depth Diameter (ft) (in) (lbs/ft) (ft) (ft) (in) 3 900 5.5 17.00 J-55 LT&C 900 900 4.767	No 75 °F 5: 198 °F 1.40 °F/100ff	ered? nperature: e temperature:	H2S conside Surface term Bottom hole	<u>Collapse:</u>				<u>se</u> I weight:	Collaps Mud		
Max anticipated surface pressure:3,216 psiInternal gradient:0.100 psi/ftTension:Non-directional string.Calculated BHP4,091 psi8 Round STC:1.80 (J)No backup mud specified.Buttress:1.60 (J)Premium:1.50 (J)Body yield:1.60 (B)Tension is based on air weight. Neutral point:True VertMax anticipated SegmentNominalRunSegmentNominalSeqLengthSizeYeightGradeFinishGradeFinishDepthDepthDiameter (ft)(in)39005.517.0039005.517.00J-55LT&C9009004.767				1.00					Ruret		
RunSegmentNominalEndTrue VertMeasuredDriftSeqLengthSizeWeightGradeFinishDepthDepthDiameter(ft)(in)(lbs/ft)(ft)(ft)(in)39005.517.00J-55LT&C9009004.767		Non-directional string.		1.80 (J) 1.60 (J) 1.50 (J) 1.60 (B) weight.	TC: : based on air	Design factor Tension: 8 Round STC: 8 Round LTC: Buttress: Premium: Body yield: Tension is based on a		: 3,216 psi dient: 0.100 psi/ft BHP 4,091 psi		Max anticipa pressure Internal grad Calculated I	
SeqLengthSizeWeightGradeFinishDepthDepthDiameter(ft)(in)(lbs/ft)(ft)(ft)(in)39005.517.00J-55LT&C9009004.767				1,703 (\$)	cost: 3 ⁻	Estimated					
3 900 5.5 17.00 J-55 LT&C 900 900 4.767	Est. Cost (\$)	Diameter	Depth	Depth		Grade	Weight		Length		
	3487	· /			LT&C		17.00		900		
	22598	4.825	7300	7300	LT&C	J-55	15.50	5.5	6400	2	
1 1450 5.5 17.00 J-55 LT&C 8750 8750 4.767	5618	4.767	8750	8750	LT&C	J-55	17.00	5.5	1450	1	
Run Collapse Collapse Collapse Burst Burst Burst Tension Tension Seq Load Strength Design Load Strength Design Load Strength (psi) (psi) Factor (psi) (psi) Factor (kips) (kips)	Tension Design Factor	Strength	Load (kips)	Design Factor	Strength (psi)	Load (psi)	Design Factor	Strength (psi)	Load (psi)	Seq	
3 421 3883 9.23 3306 5320 1.61 139.1 247	1.78 J									-	
2 3413 3927 1.15 3946 4810 1.22 123.8 217 1 4091 4910 1.20 4091 5320 1.30 24.6 247	1.75 J - 10.02 J										

Devon Energy Remarks: Date: June 19,2001 Oklahoma City, Oklahoma

Collapse is based on a vertical depth of 8750 ft, a mud weight of 9 ppg The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Engineering responsibility for use of this design will be that of the purchaser.

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