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See Rule 401 & Rule 1122

State of New Mexico
Geology, Minerals and Natural Resources Department

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

Form C-122

Revised 4-1-91

AUG 21 1996

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

Operator OXY USA				Lease or Unit Name SPIKE			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7-22-96		Well No. 1	
Completion Date 7-13-96		Total Depth 12-26		Plug Back TD 12005		Elevation	
Csg. Size 5 1/2		Wt. 17#		Set At 12005		Perforations: From: 11285 To: 11299	
Tbg. Size 2-3/8		Wt. 4.7		Set At 11050		Perforations: From: To:	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single				Packer Set At 11050		Formation	
Producing Thru tbq		Reservoir Temp. °F 172		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2	
Connection AIR		County EDDY		Pool S. Carlsbad Morrow		Meter Run 3.068	
L 11050	H 11050	Gg .619	% CO ₂ 4.73	% N ₂ .88	% H ₂ S -0-	Prover -0-	Taps 6lg

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice X Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						4180		pkc.		72 hr
1.	3.068	X 2.250	480	2	104°	3900	72	"		1 hr.
2.	3.068	X 2.250	490	6	82°	3750	74	"		1 hr.
3.	3.068	X 2.250	495	10	71°	3630	75	"		1 hr.
4.	3.068	X 2.250	490	17	63°	3390	74	"		1 hr.
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	28.78	31.40	493.2	.9602	1.271	1.038	1146
2.	28.78	54.94	503.2	.9795	1.271	1.043	2053
3.	28.78	71.28	508.2	.9896	1.271	1.047	2701
4.	28.78	92.48	503.2	.9971	1.271	1.049	3538
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	N/A	Mcf/bbl.
1.	.710	564	1.516	.929	A.P. I. Gravity of Liquid Hydrocarbons	N/A	Deg.
2.	.725	542	1.456	.919	Specific Gravity Separator Gas		XXXXXXXXXX
3.	.732	531	1.427	.912	Specific Gravity Flowing Fluid	N/A	XXXXXX
4.	.725	523	1.405	.909	Critical Pressure	694	P.S.I.A.
5.					Critical Temperature	372	R

P_c		4193.2	P_c^2		17582.9
NO.	P_i^2	P_w	P_w^2	$P_c^2 - P_w^2$	
1.		3919.0	15358.7	2224.2	
2.		3782.3	14305.6	3277.3	
3.		3676.8	13518.9	4064.0	
4.		3463.2	11993.5	5589.4	
5.					

1)

$$\frac{P_c^2}{P_c^2 - P_w^2} = \frac{3.146}{}$$

AOF = Q

$$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{11.130}{}$$

2)

$$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{3.146}{}$$

$$1) \frac{P_c^2}{P_c^2 - P_w^2} = 3.146 \quad (2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.146$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 11.130$$

Absolute Open Flow	11,130	Mcf/d @ 15.025	Angle of Slope θ	45°	Slope, n	1.000
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Remarks: NO LIQUID PRODUCED DURING TEST

Approved By Division	Conducted By: PRO WELL TESTERS	Calculated By: MB	Checked By: BM
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