

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

SEE ATTACHED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 6-3-67		JUN 20 1967	
Company TEXACO Inc.				Connection TEXACO Inc.		C. C. C.	
Pool Undesignated Wildcat				Formation Morrow		Unit	
Completion Date 6-3-67		Total Depth 19,546		Plug Back TD 15,050		Elevation	
Form or Lease Name Cotton Draw Unit							
Cas. Size 8-5/8"	Wt. 40 & 49	d 7.725	Set At 7.511	Perforations From 14,787 To 14,867		Well No. 65-1T	
Tub. Size 2-7/8"	Wt. 7.9	d 2.323	Set At 14,700	Perforations From To		Unit Sec. Twp. Rge. G 2 25S 31E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual G.G.				Packer Set At 14,700		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 208		Mean Annual Temp. °F 60		State New Mexico	
L 14,700	H 14,700	Gg 0.577	% CO ₂ 1.05	% N ₂ 0.20	% H ₂ S 0	Prover 6.065	Meter Run Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							64.77	60			12
1.	6.065		3.000	670	9.0	106	5685	84			3
2.	6.065		3.000	755	17.3	84	5190	84			3
3.	6.065		3.000	830	27.5	90	4668	86			3
4.	6.065		3.000	960	54.0	86	3108	88			3
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	44.51	78.42	683.2	.9585	1.316	1.044	4597
2	44.51	115.3	768.2	.9777	1.316	1.061	7006
3	44.51	152.3	843.2	.9723	1.316	1.064	9229
4	44.51	229.2	973.2	.9759	1.316	1.075	14084
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio DRY	Mcf/dbl.
1	1.21	566	1.64	.917	A.P.I. Gravity of Liquid Hydrocarbons	Deq.
2	1.41	544	1.58	.889	Specific Gravity Separator Gas 0.577	XX XXXXXX
3	1.53	550	1.59	.884	Specific Gravity Flowing Fluid XXXXX	0.577
4	1.78	546	1.58	.865	Critical Pressure 676 P.S.I.A.	676 P.S.I.A.
5					Critical Temperature 345 R	345 R

NO.	P _r ²	P _w	P _w ²	P _r ² - P _w ²	(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 2.3003$	(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 2.3003$
1	32469.5	5745.9	33015.4	9107.3		
2	27073.3	5313.3	28231.1	21389.1		
3	21913.4	4879.6	23810.5	51831.2		
4	9741.9	3673.3	13493.1	128629.5		
5						

Absolute Open Flow	21230	Mcf/d @ 15.025	Angle of Slope θ	45°	Slope, n	1.000
Remarks:						
Approved By Commission: _____ Conducted By: K. R. Preston, P. W. Moore						
Calculated By: P. W. Moore						
Checked By:						