

N MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-55

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 6-13-67		Well No. NM-0522	
Company PINO AMERICAN PETR. CORP.				Connection LUNO INC. GAS		Unit P	
Pool WILCOAT				Formation MORROW		Unit P	
Completion Date 6-6-67		Total Depth 16,660		Plug Back To 15,767		Elevation 3502 RDB.	
Casing Size 7"		Wt. 35'		Set At 16,526		Perforations From 14,950 To 15,010	
Tub. Size 2 1/2 EUE		Wt. 6.5'		Set At 14,422		Perforations From OPEN END To	
Type Well - Single - Broadhead - G.G. or G.O. Multiple SINGLE				Packing Set At 14,300'		County EDDY	
Producing Thru TURNING		Reservoir Temp. °F 195		Mean Annual Temp. °F 60		State N.M.	
L 14,950		H 14,950		G _g 0.571		Prover METER RUN	
%		%		%		Taps FLANGE	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							2789	91			28.33 MIN.
1.	4"	x	1.625"	525	1.5	110	3350	96			135 MIN.
2.	4"	x	1.625"	535	8.0	95	3350	100			175 MIN.
3.	4"	x	1.625"	560	19.0	96	3745	102			165 MIN.
4.	4"	x	1.625"	665	30.0	110	1275	96			
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1	15.72	38.66	546.2	0.9522	1.323	1.0381	485
2	15.79	66.20	546.2	0.9522	1.323	1.039	1120
3	15.77	104.35	573.2	0.9524	1.323	1.0411	1766
4	15.79	142.62	676.2	0.9576	1.323	1.043	2412
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.81	560	1.55	0.928	DRY GAS	0.571	XXXXXX	674	362
2	0.81	558	1.54	0.928	DRY		XXXXXX		
3	0.85	554	1.53	0.928					
4	1.01	574	1.59	0.928					
5									

NO.	P _r	P _w	P _w ² x 10 ³	P _r ² - P _w ²	(1) $\frac{P_r^2}{P_r^2 - P_w^2} =$	(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n =$
1	10777	7982	63712	6795		
2	29712	6543	42827	23683		
3	1102	4964	24641	45869		
4	1259	1510	3272	67224		
5						

$$AOF = Q \left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 2380.000$$

Absolute Open Flow 2380 scfd @ 15.025 Angle of Slope θ 55.8413 Slope, n 0.675

Remarks:

Approved By Commission:	Conducted By: H. SHAW	Calculated By: M. LANDI	Checked By: E. J. SNOOK
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