

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 6-17-70	
Company TEXACO Inc.				Connection None		
Pool Paduca Morrow				Formation Morrow		Unit
Completion Date		Total Depth 16,863	Plug Back TD 14,798	Elevation 3457 (DF)		Farm or Lease Name Cotton Draw Unit #68
Csg. Size 7.625 5.5	Wt. 10.3	d 7.625	Set At 14680	Perforations: From 14750 To 14759	Well No. 68	
Tbg. Size 2.922 2.922	Wt. 9.3	d 2.922	Set At 14150	Perforations: From To	Unit Sec. Twp. Rge. 12 25 31E	
Type Well - Single - Broadhead - G.G. or G.O. Multiple				Packer Set At 14150		County Eddy
Producing Thru Tubing		Reservoir Temp. °F 197	Mean Annual Temp. °F 14763	Baro. Press. - P _a 14150		State Dry Mexico
H 14747	G _g 14747	% CO ₂ 0.552	% N ₂ 1.00	% H ₂ S 0.00	Prover 1.006	Meter Run 718

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							7601		72 hr
1.	1" X 1.000			578	9"	95	7211	115	1 hr
2.	1" X 1.000			600	21"	105	7063	115	1 hr
3.	1" X 1.000			610	42"	112	6677	115	1 hr
4.	1" X 1.000			730	90"	108	5995	115	1 hr
5.									

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	4.753	72.94	591.2	.9680	1.348	1.030	466
2	4.753	113.48	613.2	.9592	1.348	1.029	717
3	4.753	161.78	603.2	.9534	1.348	1.028	1016
4	4.753	258.63	743.2	.9568	1.346	1.034	1640
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio Dry Mcf/bbl.	
1	0.87	555	1.66	0.943	A.P.I. Gravity of Liquid Hydrocarbons Dry Deg.	
2	0.90	565	1.69	0.943	Specific Gravity Separator Gas 0.550 X X X X X X X X	
3	0.92	572	1.71	0.947	Specific Gravity Flowing Fluid X X X X X	
4	1.10	568	1.70	0.936	Critical Pressure 677 P.S.I.A. P.S.I.A.	
5					Critical Temperature 335 R R	

NO.	P _c	P _c ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	7614.2	57979				2.00	2.6047
2			7270.2	5286	512		
3			7072.2	5002	796		
4			6690.2	4475	1323		
5			6153.2	3786	2012		

Absolute Open Flow 4,272 Mcfd @ 15.025				Angle of Slope θ	Slope, n 0.905
Remarks:					
Approved By Commission:		Conducted By: Lednicki - Preston		Calculated By: Lee	
Checked By:					