

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 6/23/72		NOV 1 1972	
Company Black River Corporation				Connection			
Pool Washington Ranch				Formation Upper Morrow		Unit O.G.C. ARTESIA, OFFICE	
Completion Date 6/11/72		Total Depth 7125		Plug Back TD 7075		Elevation 3780 KB	
Csg. Size 5 1/2		Wt. 15.5		Set At 7125		Perforations: From 6953 To 6954	
Thq. Size 2 7/8		Wt. 6.5		Set At 6975		Perforations: From Open To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G.G. Multiple				Packer Set At 6975		County Eddy	
Producing Thru Casing		Reservoir Temp. °F 148_a 6985		Mean Annual Temp. °F 60°F		Baro. Press. - P _a 13.2	
L 6953		H 6953		G _g 0.657		% CO ₂ -	
						% N ₂ -	
						% H ₂ S -	
				Prover		Meter Run 4"	
						Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							Choke		2481	89	72
1.	4"	x	2.25	550	4	91	15/64		2184	82	2
2.	4"	x	2.25	488	14	97	20/64		2024	82	2
3.	4"	x	2.25	515	39	102	30/64		1669	82	2
4.	4"	x	2.25	540	61	100	42/64		1326	82	2
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	25.64	47.46	563.2	.9715	1.234	1.048	1529
2	25.64	83.77	501.2	.9662	1.234	1.041	2663
3	25.64	143.53	528.2	.9619	1.234	1.042	4552
4	25.64	183.70	553.2	.9636	1.234	1.045	5853
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	TSTM	Mcf/bbl.
1	0.84	551	1.47	.910	A.P.I. Gravity of Liquid Hydrocarbons		
2	0.75	557	1.49	.923	Specific Gravity Separator Gas	0.657	XXXXXX
3	0.79	562	1.50	.921	Specific Gravity Flowing Fluid	XXXXX	
4	0.83	560	1.49	.916	Critical Pressure	670	P.S.I.A.
5					Critical Temperature	375	R

NO.	P _c	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	2494.2	6221			1.419	1.419
1		2197.9	4831	1390		
2		2039.3	4158	2063		
3		1689.7	2855	3366		
4		1355.3	1837	4384		
5						

Absolute Open Flow 8305		Mcf/d @ 15.025		Angle of Slope θ		Slope, n 1.000	
Remarks:							
Approved By Commission:		Conducted By:		Calculated By: <i>Donna Hollas</i>		Checked By:	