

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65
132

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7-14-75		JUL 28 1975	
Company Texas Pacific Oil Co., Inc.				Connection None		O. C. C.	
Pool Wildcat				Formation Wolfcamp		ARTESIA, OFFICE	
Completion Date 7-15-75		Total Depth 16,976		Perforations: 13,725		Elevation 3188 GL	
Csg. Size 7 5/8"		Wt. 39#/ft.		Set At 6,625		Perforations: From 12,670' To 12,698'	
Tbg. Size 3 1/2"		Wt. 12.95#/ft.		Set At 2.75"		Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 12,487'		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 251° @ 12,487'		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2	
L 12,670		H 12,670		G _g .640		% CO ₂ .12	
				% N ₂ .66		% H ₂ S 0	
				Prover		Meter Run 4.026	
						Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI									Packer		
1.	4.026		2.25	690	12	110	8187				60 Min.
2.	4.026		2.25	740	30	105	7980				"
3.	4.026		2.25	957	66	91	7217				"
4.	4.026		2.25	1185	78	85	6067				"
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	25.64	91.8608	703.2	.9551	1.250	1.054	2963
2.	25.64	150.320	753.2	.9594	1.250	1.056	4881
3.	25.64	253.048	970.2	.9715	1.250	1.080	8509
4.	25.64	305.712	1198.2	.9768	1.250	1.101	10537
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	1.050	570	1.532	.901	283.6	55.2° @ 60°	.640	X X X X X X X X	670	372
2.	1.124	565	1.519	.896			X X X X X			
3.	1.448	551	1.481	.857						
4.	1.788	545	1.465	.825						
5.										

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1.	10100	9907	98148.6	3861.4	26.418	6.6788
2.		9665	93412.2	8597.8		
3.		8920	79566.4	22443.6		
4.		7842	61497.0	40513.0		
5.						

Absolute Open Flow 19,789 Mcfd @ 15.025		Angle of Slope @ 30.1°		Slope, n .580	
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Remarks: PW substituted for P _t - Measured with Amerada Inst. No. 34044 w/12,500# element at 12487', pressures extrapolated to 12684' (Mid Perf)	
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Approved By Commission:	Conducted By:	Calculated By:	Checked By:
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