

MULTIPOINT, AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

AMENDED REPORT

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Form C-122
Revised 9-1-65

OCT 7 1975

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10-2-75			
Company Skelly Oil Company				Connection Pending				O.C.C. ARTECIA, OFFICE	
Pool Wildcat				Formation Lower Penn				Unit	
Completion Date 8-4-75		Total Depth 15,120'		Plug Back TD 14,660'		Elevation 3475 GR		Farm or Lease Name Todd 2 State	
Csg. Size 5" Liner	Wt. 23.60	d 4.000	Set At 14,966'	Perforations: From 13,508' To 14,622'		Well No. 1			
Tub. Size 2-7/8	Wt. 6.5	d 2.441	Set At 11,968'	Perforations: From - To -		Unit F	Sec. 2	Twp. 24	Rge. 31
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 11,968'		County Eddy			
Producing Thru Tubing		Reservoir Temp. °F 8		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L 14,065	H 14,065	G _g .586	% CO ₂ .73	% N ₂ 1.07	% H ₂ S -	Prover -	Meter Run 4"	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4		1	360	36"	73	394	65	Packer		2
2.	4		1	370	26"	67	521	58			2
3.	4		1	360	23"	64	728	57			2
4.	4		1	310	17"	80	1350	54			4
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	4.7524	115.9	373.2	.9877	1.306	1.027	730
2.	4.7524	99.8	383.2	.9933	1.306	1.029	633
3.	4.7524	92.6	373.2	.9962	1.306	1.028	589
4.	4.7524	74.1	323.2	.9813	1.306	1.022	462
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.	.55	533	1.54	.949	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	.57	527	1.52	.945	Specific Gravity Separator Gas .586 X X X X X X X X
3.	.55	524	1.51	.946	Specific Gravity Flowing Fluid X X X X X
4.	.48	548	1.56	.957	Critical Pressure 675 P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature 342 R _____ R

P _c 6169.2 P _c ² 38059.0					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.00$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.00$
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 733$	
1		415.8	172.9	37886		
2		539.0	290.6	37768		
3		744.4	554.2	37505		
4		1365.6	1865.0	36194		
5						

Absolute Open Flow 733 Mcfd @ 15.025		Angle of Slope 45.0	Slope, n 1.000
Remarks:			
Approved By Commission:		Conducted By: Joe Banks	Calculated By: Jerrel Marburger
		Checked By:	