

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT A ONE POINT BACK PRESSURE TEST OR GAS WELL

Form C-122
Revised 9-1-65
C-122

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 5-16-79		JUN 4 1979	
Company AMOCO PRODUCTION COMPANY ✓				Connection EL PASO NATURAL GAS COMPANY		O.C.C.	
Pool UNDESIGNATED				Formation MORROW		ARTESIA, OFFICE	
Completion Date 2-9-79		Total Depth 13026.		Plug Back TD 13026.		Elevation 3009.	
Form or Lease Name WILLIAMS GAS COMPANY							
Csg. Size 5.000	Wt. 18.0	d 4.276	Set At 13026.	Perforations: From 12492. To 12763.		Well No. 1	
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 12358	Perforations: From 0. To 0.		Unit Sec. Twp. Rge. C 25 23S 28E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 9744.		County EDDY	
Producing Thru TUBING		Reservoir Temp. °F 206. @ 12627.		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2	
State NEW MEXICO							
L 12627.	H 12627.	G _g 0.574	% CO ₂ 0.68	% N ₂ 0.74	% H ₂ S 0.	Prover 0.	Meter Run 4.0
						Taps FLANGE	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SE							1685.	72			44.0
1.	4.03 x 1.250			611.	2.2	76.	1639.	76.	0.	0.	1.0
2.	4.03 x 1.250			611.	6.2	75.	1581.	80.	0.	0.	1.0
3.	4.03 x 1.250			611.	12.2	71.	1515.	80.	0.	0.	1.0
4.	4.03 x 1.250			611.	18.5	72.	1435.	82.	0.	0.	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _L	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	7.47	37.48	624.2	0.9850	1.3199	1.0437	380.
2	7.47	62.46	624.2	0.9859	1.3199	1.0440	634
3	7.47	87.44	624.2	0.9896	1.3199	1.0454	892
4	7.47	107.43	624.2	0.9887	1.3199	1.0450	1094.
5.							

NO.	P _c	Temp. °F	T _g	Z	Gas Liquid Hydrocarbon Ratio	A.P.L. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.92	536.	1.54	0.918	0	0	0.574	X X X X X X X X	676.	347.
2.	0.92	535.	1.54	0.917				X X X X X		
3.	0.92	531.	1.53	0.915						
4.	0.92	532.	1.53	0.916						
5.										

NO.	P _c	P _w	P _w ²	P _c ² - P _w ²
1	2730.	1643.	2699.	161.
2	2541.	1583.	2506.	354.
3	2335.	1518.	2305.	554.
4	2097.	1439.	2069.	790.
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.6199$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2580.$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.3576$

Absolute Open Flow	2580.	Mcfd @ 15.025	Angle of Slope θ	56.3	Slope, n	0.667
Remarks:						

Approved By Commission:	Conducted By: John West Engr.	Calculated By: C.C. Weaver	Checked By: W.D. Magness
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3 - NMOC D-A

1 - WDM

1 - Robert Coleman

1 - Div
1 - SUCO

1 - DLB

1 - Maddox