MEXICO OIL CONSERVATION C ON

MULTIPOINT AND ONE POINT BACK PRESSURE TES, FOR GAS WELL

C-5F

Form C-122
Revised 9-1-65

RECEIVED

JUN 20 1980

O. C. D.

ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 05-22-80	
Company: SUPERIOR OIL Co.			Connection: AIR		
Pool: WILDCAT			Formation: MORROW		Unit
Completion Date: 05-20-80	Total Depth: 11968		Plug Back TD: 11786	Elevation: 3449.4 KB	Farm or Lease Name: DELTA FEDERAL
Csg. Size: 7-5/8 +	Wt.: 5" liner	d	Set At: 8835-11968	Perforations: From ~~11335~~ 11333 To ~~11356~~ 11354	Well No.: #1
Tbg. Size: 2-7/8" &	Wt.: 2-3/8"	d	Set At: 8700-11100	Perforations: From To	Unit: Sec. 7, Twp. 25, Rge. 26
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE GAS			Packer Set At: 11100		County: EDDY
Producing Thru: Tubing	Reservoir Temp. °F: 188 @ 11440		Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11440	11440	.5721	.865	.495			4"	Flg.

	FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						3925				24 Hr.
1.	4	x 1.500	610	3.0	110	3760				1 Hr.
2.	4	x 1.500	615	8.0	112	3570				1 Hr.
3.	4	x 1.500	615	15.0	108	3300				1 Hr.
4.	4	x 1.500	615	24.5	104	2980.				1 Hr.
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	10.84	43.24	623.2	.9551	1.322	1.033	611
2.	10.84	70.89	628.2	.9535	1.322	1.033	1001
3.	10.84	97.07	628.2	.9568	1.322	1.034	1376
4.	10.84	124.06	628.2	.9602	1.322	1.035	1767
5.							

NO.	P_t	Temp. °R	T_r	Z
1	.93	570	1.65	.937
2.	.93	572	1.65	.937
3.	.93	568	1.64	.935
4.	.93	564	1.63	.933
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.

A.P.I. Gravity of Liquid Hydrocarbons Dry Deg.

Specific Gravity Separator Gas .5721 XXXXXXXXX

Specific Gravity Flowing Fluid XXXXX

Critical Pressure 672 P.S.I.A. _____ P.S.I.A.

Critical Temperature 346 R _____ R

P_c 3948.2 P_c^2 15588.3

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	4763.2	3815.5	14558.0	1030.3
2	4549.2	3631.9	13190.4	2397.9
3	4263.2	3389.1	11486.3	4102.0
4	3911.2	3094.9	9578.3	6010.0
5	4900.2	S.I.P.		

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.594$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.751$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3.095$

Absolute Open Flow 3095 Mcfd @ 15.025 Angle of Slope θ 59.5 Slope, n .588

Remarks: B.H.P. Taken from a bomb set at 11440'.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	DAVIS SERVICES, INC.	RICK PAGAN	F.E. FLORES