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C-122 Revised 9-1-65

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NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

JUN 25 1982

O. C. D.
ARTESIA, OFFICE

Type Test: XX Initial ☐ Annual ☐ Special	Test Date: 6-7-82		
Company: Bass ~~Enterprises~~	Connection: Air		
Pool:	Formation: Lower Morrow	Unit:	
Completion Date: 6-3-82	Total Depth: 15530	Plug Back TD: 15483	Elevation: 3390 GL
Farm or Lease Name: Poker Lake	Well No.: 53		
Csg. Size: 5"	Wt.:	d:	Set At: 15530
Perforations: From 15440 To 15456			
Tbg. Size: 2 3/8	Wt.:	d:	Set At: 15418
Perforations: From To			
Unit:	Sec.: 9	Twp.: 25S	Rge.: 31E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single Gas	Packer Set At: 15390	County: Eddy	
Producing Thru: Tbg.	Reservoir Temp. °F: 228 @ 15418	Mean Annual Temp. °F: 60°	Baro. Press. – P_a: 13.2
State: New Mexico			
L: 15418	H: 15418	Gg: .5862	% CO_2: 1.993
% N_2: 2.256	% H_2S:	Prover:	Meter Run: 4"
Taps: Flg.			

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					6600				72 hr.
1.	4 X 1.000	570	11.0	126	5900				1 hr.
2.	4 X 1.000	570	24.0	126	5500				1 hr
3.	4 X 1.000	570	66.0	120	4600				1 hr.
4.	4 X 1.500	575	19.0	100	3675				1 hr.
5.	4 X 1.500	530	23.0	102	2490				4 hr.

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.753	80.09	583.2	.9420	1.306	1.030	482
2	4.753	118.31	583.2	.9420	1.306	1.030	713
3.	4.753	196.19	583.2	.9469	1.306	1.033	1191
4.	10.84	105.72	588.2	.9636	1.306	1.038	1497
5.	10.84	111.77	543.2	.9619	1.306	1.034	1574

NO.	P_r	Temp. °R	T_r	Z
1.	.87	586	1.66	.943
2.	.87	586	1.66	.943
3.	.87	580	1.64	.938
4.	.88	560	1.58	.929
5.	.81	562	1.59	.935

Gas Liquid Hydrocarbon Ratio: dry Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: XXXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 672 P.S.I.A. P.S.I.A.
Critical Temperature: 354 R R

P_c 6613.2 P_c^2 43734.4

NO	BHP	P_w	P_w^2	$P_c^2 - P_w^2$
1	7587.2	5948.6	35386.3	8348.1
2	7147.2	5556.9	30879.1	12855.3
3	6141.2	4681.6	21917.1	21817.3
4	5054.2	3767.5	14193.9	29540.5
5	3643.2	2647.7	7010.4	36724.0
	8334.2 S.I.P.			

(1) $\frac{P_c^2}{P_c^2 - P_w^2}$ = 1.480

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 1.412

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 2.114

Posted ID Comp Book 7-2-82 SI

Absolute Open Flow: 2,114 Mcfd @ 15.025
Angle of Slope θ: 48.75°
Slope, n: .880

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Davis Services, Inc.	Rick Pagan	