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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Burlington Resources Oil & Gas Company Lease or Unit Name Meridian 16 state

Type Test ☒ Initial ☐ Annual ☐ Special Test Date 4-19-99 Well No. 15001

Completion Date 3-2-99 Total Depth 13309 Plug Back TD 13021 Elevation 3212' Twp. - Sec. - TWP. - Rge. 16 - 26-5 - 31-E

Cg. Size 7" Wt. 26# d 6.276 Set At 12,214' Perforations: From: 12664 To: 13021 County Eddy

Tbg. Size 2 7/8 Wt. 6.5 d 2.441 Set At 11921 Perforations: From: 11921 To: 13021 Pool Phantom Draw

Type Well - Single - Bradenhead - G.O. - G.O. Multiple Single - Horizontal Packer Set At 11921 Formation Wolfcamp

Producing Thru tbg Reservoir Temp. °F 193.5 Mean Annual Temp. °F 60 Baro. Press. - P. 13.2 Connection Sales

L 11950 II 11950 Gg .696 % CO₂ .289 % N₂ .510 % H₂S 0 Prover 0 Meter Run 4.026 Taps flg

FLOW DATA

NO.	Prover Line Size	X	Orifice Size	Press. psig.	Diff. h _w	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. psig.	Temp. °F	Press. psig.	Temp. °F	
1.	2.00 x 4.026			89	8.1	88 ⁰	4580		pkg		60 min
2.	2.00 x 4.026			174	10.8	75 ⁰	4420		pkg		
3.	2.00 x 4.026			275	18.2	63 ⁰	4280		pkg		
4.	2.00 x 4.026			310	22.0	55 ⁰	4110		pkg		
5.							3680		pkg		

RATE OF FLOW CALCULATIONS

NO.	COEFFICIENT (24 HOUR)	$h_w P_m$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor F _{sp}	Rate of Flow Q, Mcfd
1.	19.81	28.7	102.2	.9741	1.199	1.053	699
2.	19.81	44.9	187.2	.9859	1.199	1.056	1110
3.	19.81	72.4	288.2	.9971	1.199	1.060	1817
4.	19.81	84.3	323.2	1.005	1.199	1.062	2137

NO.	P _i	Temp. °R	T _i	Z	Gas Liquid Hydrocarbon Ratio	N/A	Method
1.	.81	548	1.42	.902	A.P. I. Gravity of Liquid Hydrocarbons	N/A	Deg.
2.	.79	535	1.39	.896	Specific Gravity Separator Gas	.696	XXXXXXXXXX
3.	.77	523	1.36	.890	Specific Gravity Flowing Fluid	XXXXXX	
4.	.76	515	1.34	.886	Critical Pressure	672	PSIA
5.					Critical Temperature	384	R

P_e 4593.2 P_w 21097.5

NO.	P _i ²	P _w ²	P _e ²	P _e ² - P _w ²
1.		4434.1	19661.0	1436.5
2.		4295.4	18450.6	2646.9
3.		4129.2	17050.7	4046.8
4.		3702.0	13704.9	7392.5

$$1) \frac{P_e^2}{P_e^2 - P_w^2} = \frac{2.85}{\frac{P_e^2}{P_e^2 - P_w^2}} \quad (2) \left[\frac{P_e^2}{P_e^2 - P_w^2} \right]^a = \frac{2.11}{\left[\frac{P_e^2}{P_e^2 - P_w^2} \right]}$$

$$AOF = Q \left[\frac{P_e^2}{P_e^2 - P_w^2} \right]^a = \frac{4.518}{\left[\frac{P_e^2}{P_e^2 - P_w^2} \right]}$$

Absolute Open Flow 4,518 Mcfd @ 15.025 Angle of Slope θ 54.44 Slope, n .714

Remarks: *No liquid made during test

Approved By Division _____ Conducted By: Pro Well Testing Calculated By: MB Checked By: BM